Supporting Information

This appendix provides the explicit mathematical expressions to be plugged in the equations presented in $\S2.6$ to determine the traction stresses. These formulae should be preferred to those in the Supporting Information of del Álamo *et al.* [13]. The latter were particularized to two-dimensional boundary conditions and contained a number of typographical errors that have been corrected here. The resolvant matrix of the Fourier transform of the elastostatic equation is

$$\mathbf{U}(\alpha,\beta,z) = \begin{bmatrix} \frac{\alpha^2 z \cosh(kz)}{4k^2(1-\sigma)} + \frac{[4(1-\sigma)k^2 - \alpha^2]\sinh(kz)}{4k^3(1-\sigma)} \\ \frac{\alpha\beta z \cosh(kz)}{4k^2(1-\sigma)} - \frac{\alpha\beta \sinh(kz)}{4k^3(1-\sigma)} \\ \frac{-i\sinh(kz)z\alpha}{4k(1-\sigma)} \end{bmatrix}$$
(22)

$$\mathbf{V}(\alpha,\beta,z) = \begin{bmatrix} \frac{\alpha\beta z \cosh(kz)}{4k^2(1-\sigma)} - \frac{\alpha\beta \sinh(kz)}{4k^3(1-\sigma)} \\ \frac{\beta^2 z \cosh(kz)}{4k^2(1-\sigma)} + \frac{[4(1-\sigma)k^2-\beta^2]\sinh(kz)}{4k^3(1-\sigma)} \\ \frac{-i\sinh(kz)z\beta}{4k(1-\sigma)} \end{bmatrix}$$
(23)
$$\mathbf{W}(\alpha,\beta,z) = \begin{bmatrix} \frac{-i\alpha z \sinh(kz)}{2k(1-2\sigma)} \\ \frac{-i\beta z \sinh(kz)}{2k(1-2\sigma)} \\ \frac{-z\cosh(kz)}{2k(1-2\sigma)} + \frac{(3-4\sigma)\sinh(kz)}{2k(1-2\sigma)} \end{bmatrix}.$$
(24)

The inverse of the resolvant matrix particularized at the surface of the substratum is given by

$$\begin{bmatrix} \mathbf{U}_{mn}(h) & | \mathbf{V}_{mn}(h) & | \mathbf{W}_{mn}(h) \end{bmatrix}^{-1} = \begin{bmatrix} C_{1u} & C_{1v} & C_{1w} \\ C_{2u} & C_{2v} & C_{2w} \\ C_{3u} & C_{3v} & C_{3w} \end{bmatrix},$$
(25)

where

$$\begin{split} C_{1u} &= \frac{\left(-4\beta^2 h^2 + 2 \left(-3 + 4\,\sigma\right)^2 (\cosh(2\,k\,h) - 1)\right) k^5 + 8\,\alpha^2 h\,(-1 + \sigma)\sinh(2\,k\,h) k^4 - 2\,\alpha^2 (\cosh(2\,k\,h) - 1)(-3 + 4\,\sigma) k^3}{k^4 \left(4\,h^2 k^2 + 3\,(-3 + 4\,\sigma)^2\right)\sinh(k\,h) - (-3 + 4\,\sigma)^2 k^4\sinh(3\,k\,h)}, \\ C_{1v} &= \frac{4\,\alpha\,k^5 h^2 \beta + 8\,\alpha\,\beta\,h\,(-1 + \sigma)\sinh(2\,k\,h) k^4 + (-2\,\alpha\,\beta\,(-3 + 4\,\sigma)\cosh(2\,k\,h) + 2\,\alpha\,\beta\,(-3 + 4\,\sigma)) k^3}{k^4 \left(4\,h^2 k^2 + 3\,(-3 + 4\,\sigma)^2\right)\sinh(k\,h) - (-3 + 4\,\sigma)^2 k^4\sinh(3\,k\,h)}, \\ C_{1w} &= \frac{-8\,i k^5 \alpha\,(-1 + \sigma)h\,(\cosh(2\,k\,h) - 1)}{k^4 \left(4\,h^2 k^2 + 3\,(-3 + 4\,\sigma)^2\right)\sinh(k\,h) - (-3 + 4\,\sigma)^2 k^4\sinh(3\,k\,h)}, \\ C_{2u}(\alpha,\beta) &= C_{1v}(\beta,\alpha), \\ C_{2v}(\alpha,\beta) &= C_{1v}(\beta,\alpha), \\ C_{2w}(\alpha,\beta) &= C_{1w}(\beta,\alpha), \\ C_{2w}(\alpha,\beta) &= C_{1w}(\beta,\alpha), \\ C_{3u}(\alpha,\beta) &= \frac{-4i\alpha\,(-1 + 2\,\sigma)h\,\sinh(k\,h) k^3}{(-3 + 4\,\sigma)^2 k^2\cosh(2\,k\,h) - 2\,h^2 k^4 - (-3 + 4\,\sigma)^2 k^2}, \end{split}$$

$$C_{3v}(\alpha,\beta) = C_{3u}(\beta,\alpha),$$

$$C_{3w} \frac{-4k^4h(-1+2\sigma)\cosh(kh)+4\sinh(kh)(-1+2\sigma)(-3+4\sigma)k^3}{(-3+4\sigma)^2k^2\cosh(2kh)-2h^2k^4-(-3+4\sigma)^2k^2}.$$

Finally, the linear operator that defines Hooke's law in Fourier space can be written as

$$\mathcal{H} = \frac{E}{2(1+\sigma)} \begin{bmatrix} 0 & 0 & i\alpha_m & 1 & 0 & 0\\ 0 & 0 & i\beta_n & 0 & 1 & 0\\ \frac{2i\alpha_m\sigma}{(1-2\sigma)} & \frac{2i\beta_n\sigma}{(1-2\sigma)} & 0 & 0 & 0 & \frac{2(1-\sigma)}{(1-2\sigma)} \end{bmatrix}.$$
 (26)

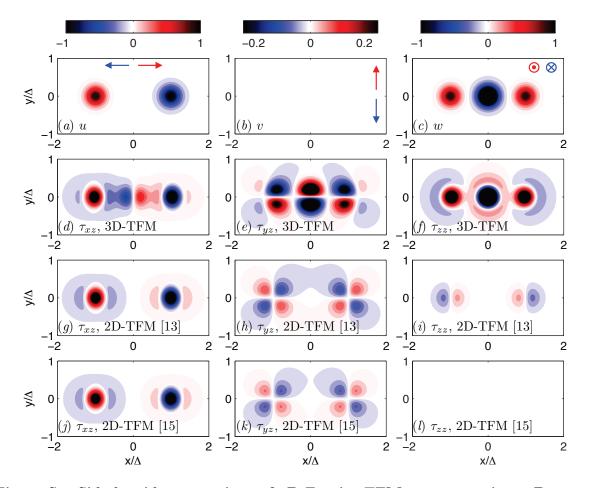


Figure S1. Side by side comparison of 3D Fourier TFM versus previous 2D methods [13,15] for a synthetic deformation field representative of the deformation pattern exerted by migrating amoeboid cells. The Poisson's ratio is $\sigma = 0.3$ and the substratum thickness, $h = 2\Delta$, is equal to the length of the "synthetic cell". The plots in the top row show the synthetic deformation field in the x direction (eq. 11, panel a), y direction (zero, panel b) and z direction (eq. 13, panel c). The second row shows the traction stresses calculated from the displacements in panels (a)-(c) by 3D Fourier TFM. (d), τ_{xz} ; (e), τ_{yz} ; (f), τ_{zz} . The third row shows the traction stresses calculated from the displacements on the substratum's surface (i.e. w(z = h) = 0 as in ref. [15]). (g), τ_{xz} ; (h), τ_{yz} ; (i), τ_{zz} . The last row shows the traction stresses calculated from the displacements in panels (a)-(c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (c) by 2D Fourier TFM under the assumption of zero normal stresses on the substratum's surface (i.e. τ_{zz} (z = h) = 0 as in ref. [13]). (j), τ_{xz} ; (k), τ_{yz} ; (l), τ_{zz} .

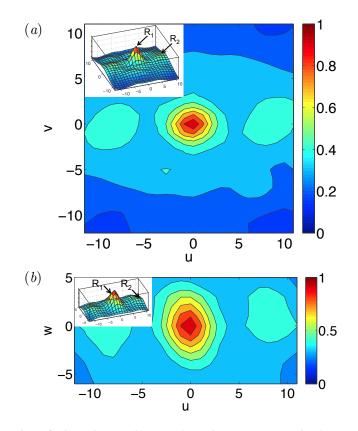


Figure S2. Example of the three-dimensional cross-correlation of fluorescence intensity, R(u, v, w), for a pair of interrogation boxes of size $24 \times 24 \times 12$ in the x, yand z directions. The three-dimensional location of the peak of the cross-correlation yields the relative displacement between the two interrogation boxes. The signal-to-noise ratio in this example, s2n = 2.22, is determined by the ratio of the maximum value of the cross-correlation $(R_1 = 1)$ to the second highest local maximum $(R_2 = 0.45)$. (a), Contour map of a two-dimensional section of the cross-correlation for zero displacement in the z direction, R(u, v, w = 0). (b), Contour map of a two-dimensional section of the cross-correlation for zero displacement in y direction, R(u, v = 0, w). The insets in both panels are height maps of each two-dimensional section of R(u, v, w).

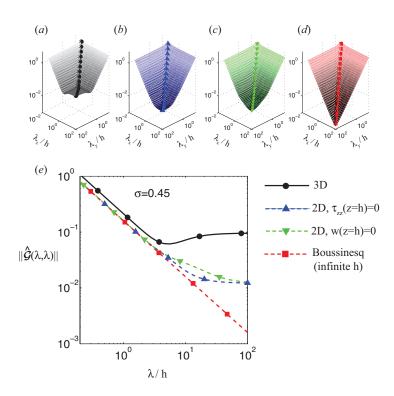


Figure S3. Fröbenius norm of the Green's function used by different TFM methods, $||\hat{\mathcal{G}}||$ (eq. 20), for a value of the Poisson's ratio $\sigma = 0.45$. The four panels in the top row (a-d) show surface plots of $||\hat{\mathcal{G}}||$ as a function of the horizontal wavelengths of the deformation field (λ_x, λ_y) . (a), present 3D TFM method; (b), 2D TFM under the assumption of zero normal stresses on the substratum's surface (i.e. $\tau_{zz}(z=h)=0$ as in ref. [13]); (c), 2D TFM under the assumption of zero normal displacements on the substratum's surface (i.e. w(z=h)=0 as in ref. [15]); (d), Boussinesq's traction cytrometry assuming infinitely-thick substratum (as in refs. [10, 12]). The symbol curves in these plots indicate the sections of $||\hat{\mathcal{G}}||$ represented in panel (e). (e), $||\hat{\mathcal{G}}||$ along the line $\lambda = \lambda_x = \lambda_y$ from different TFM methods, represented as a function of λ/h .