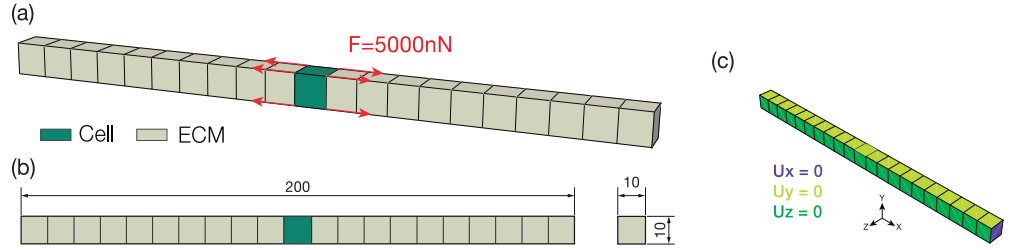


## S1 File

### A benchmark problem for inverse analysis in TFM

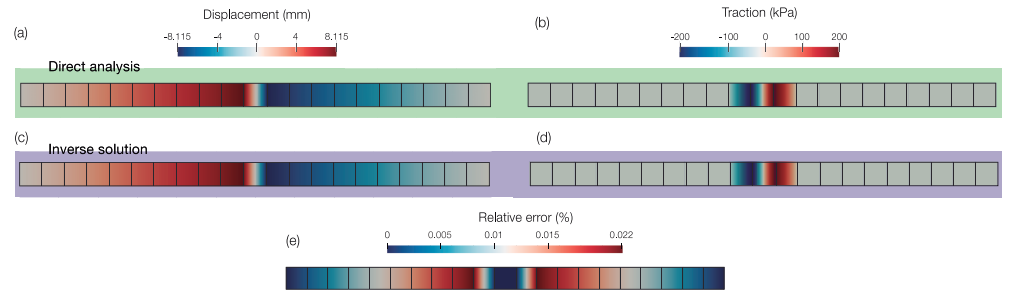
To further test the methodology proposed, a benchmark problem is numerically discussed. We implement a uniaxial traction test, where some forces are applied in the central nodes simulating the forces exerted by one cell in the longitudinal direction. The model consists of one  $200 \times 10 \times 10 \mu\text{m}$  bar discretised into 21 voxels (see Fig. S3). The central voxel represents one cell (element in dark green), while the remaining 20 voxels, 10 to each side, simulate the ECM. We assume that both cell and ECM behave as hyperelastic Neo-Hookean isotropic materials. In this analysis, we set the value of the parameters  $C_{10}$  and  $D_1$  to  $23.077 \text{ kPa}$  and  $0.02 \text{ kPa}^{-1}$  respectively for the cell and  $2.3077 \text{ kPa}$  and  $0.2 \text{ kPa}^{-1}$  for the ECM. A force of  $5000 \text{ nN}$  is imposed to each of the eight nodes of the cell voxel as shown in Figure S3. Boundary conditions were fixed in order to simulate a uniaxial problem in which the cross section area is not allowed to change its shape. Thus, the displacements only occur in the longitudinal direction. The maximum displacement obtained in the direct analysis was  $8.115 \mu\text{m}$ , which occurs in the cell.



**Fig S3. Uniaxial traction benchmark analysis.** (a) Geometry of the model. In dark green colour, the voxel representing a cell, in light green those voxels simulating the ECM. Forces due to cell activity are imposed to each of the cell nodes (red arrows). (b) Dimensions of the model in microns. (c) Boundary conditions applied during the analysis. Both y and z displacements are forced to be zero. At the ends of the bar, the x-displacement is prevented to avoid the movement as a rigid solid.

The resulting displacement field in the ECM obtained from the forward problem, was used as input for the inverse method analysis. After running six iterations, the analysis reached convergence, obtaining a maximum displacement of  $8.11467 \mu\text{m}$  in the cell. The maximum relative error measured in displacements was  $0.022\%$ . Figure S4 summarizes the results obtained in this benchmark problem.

In the TFM analysis, the aim is to obtain the traction forces to relate them with the forces exerted by cells. However, it is important to distinguish among the different variables related to the mechanical effort exerted or sensed by cells and ECM that can be numerically computed: the forces exerted by the cell, surface tractions (force per area), the stress sensed by the cell and the strains of both cell and ECM. Therefore, it is essential to define the specific output or variable that we aim to recover from this inverse analysis. The straightforward result is obtaining the strains experienced by the ECM. For example, Peñas *et. al.* [1] recovered the Green-Lagrange strain tensor in the



**Fig S4. Uniaxial traction benchmark analysis.** (a) Displacement obtained in the direct analysis. (b) Traction imposed in the direct analysis. (c) Displacement recovered after running the inverse method. (d) Traction recovered in the inverse analysis. (e) Relative error obtained measured in displacements. Maximum errors are located close to the cell and their value is 0.022%.

ECM. Using the strain tensor and the energy deformation function, the stress tensor can be also computed in the ECM. Firstly, using the density energy function of the ECM, the stress exerted by the ECM into the cell is calculated. Similarly, if the cell mechanical properties are known, using the density energy function of the cell, the stress exerted by the cell into the ECM is obtained. Thus, only the second one is taken into account since the aim of the TFM inverse methodology is to obtain the forces exerted by the cell. After computing the stress tensor, another output available is the surface traction forces. These output is obtained in the majority of the inverse methods presented in the literature [2–4]. To obtain surface tractions it is necessary to calculate the normal vectors to the planar surface. Concentrated forces can be calculated, but in this case the area of each element has to be obtained. Following the assumption that two different stress tensors can be computed ( $\sigma_{ECM \rightarrow cell}$ , the stress the ECM exerts on the cell and  $\sigma_{cell \rightarrow ECM}$ , the stress the cell exerts on the ECM), also two different forces can be calculated. The sum of both forces represents the total forces exerted by the cell.

Following this benchmark problem, all these outputs can be easily checked. Since the problem is uniaxial, only the longitudinal direction results are shown. After performing the inverse analysis, the stress obtained is distributed between the cell and the ECM:  $\sigma_{ECM \rightarrow cell} = -1.438$  kPa and  $\sigma_{cell \rightarrow ECM} = 198.561$  kPa. Therefore, the force applied by the cell in the interface between the cell and the ECM, since there is no change in the cross section area due to boundary conditions is equal to 19999.96 nN, i.e. 4999.99 nN per node.

## References

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