

RESEARCH ARTICLE

A coarse-grained red blood cell membrane model to study stomatocyte-discocyte-echinocyte morphologies

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Abstract

An improved red blood cell (RBC) membrane model is developed based on the bilayer coupling model (BCM) to accurately predict the complete sequence of stomatocyte-discocyte-echinocyte (SDE) transformation of a RBC. The coarse-grained (CG)-RBC membrane model is proposed to predict the minimum energy configuration of the RBC from the competition between lipid-bilayer bending resistance and cytoskeletal shear resistance under given reference constraints. In addition to the conventional membrane surface area, cell volume and bilayer-leaflet-area-difference constraints, a new constraint: total-membrane-curvature is proposed in the model to better predict RBC shapes in agreement with experimental observations. A quantitative evaluation of several cellular measurements including length, thickness and shape factor, is performed for the first time, between CG-RBC model predicted and three-dimensional (3D) confocal microscopy imaging generated RBC shapes at equivalent reference constraints. The validated CG-RBC membrane model is then employed to investigate the effect of reduced cell volume and elastic length scale on SDE transformation, to evaluate the RBC deformability during SDE transformation, and to identify the most probable RBC cytoskeletal reference state. The CG-RBC membrane model can predict the SDE shape behaviour under diverse shape-transforming scenarios, in-vitro RBC storage, microvascular circulation and flow through microfluidic devices.

Introduction

Red blood cell (RBC) is a unique cell without any nucleus or mitochondria [1–3] and is remarkably simple in its structure. The most important function of RBC is the transfer of oxygen to body tissues and RBC is adapted with many features to maximize its performance as a gas carrier. It is extremely deformable and elastic to sustain its passage through narrow

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capillaries of the microvasculature [3, 4]. RBC holds ~ 40% excess surface area as compared to a sphere with the same volume [2, 5], and the higher surface area allows an increased gas transfer across its surface [6]. The structural integrity and the stability of the RBC is due to its membrane which is comprised of three main components; the phospholipid bilayer, transmembrane proteins and the cytoskeleton [4, 7]. The cytoskeleton is mainly composed of spectrin tetramers connected at actin junctional complexes in a triangular network form [7, 8], and is the major contributor to the highly elastic nature of the RBC, whereas the lipid bilayer contributes to the viscosity and area preserving nature of the RBC [9, 10].

It has been found that the normal biconcave shape of RBC can be modified into stomatocytes and echinocytes through variety of agents, some of them such as amphipaths, extracellular ionic strength and pH, causing reversible transformations at constant membrane surface area and cell volume [11–16]. Stomatocytes are cup-like concave shapes whereas echinocytes are crenated shapes with a spiculated cell surface [9, 12–15, 17]. Stomatocytes and echinocytes shapes are further categorized into subclasses I, II, III and IV considering different stages of concavity and crenation. The Bessis' nomenclature is commonly used to identify different RBC shapes [18], and the different stages of stomatocyte-echinocyte can be described as follows. Stomatocyte I is a cup shape with a shallow circular invagination; Stomatocyte II is a cup shape with a deeper invagination, still at least approximately circular; Stomatocyte III is a cup shape with a deep invagination, often elongated into a mouth-like slit and sometimes accompanied by other pit-like invaginations; Sphero-stomatocyte (Stomatocyte IV) is a spherical shape with small interior buds still attached to the membrane; Echinocyte I is a disc with several undulations around its rim; Echinocyte II is a flattened elliptical body with rounded spicules distributed more or less uniformly over its surface; Echinocyte III is an ovoid or spherical body with sharper and more numerous (30–50) spicules distributed evenly over its surface; and Sphero-echinocyte (Echinocyte IV) is a sphere with small sharp projections still attached to its surface [19]. Refer to Fig 1 for a representation of RBC morphology at different stages of stomatocytosis and echinocytosis.

Among the identified many physical and chemical conditions, cationic amphipaths, low salt, low pH and cholesterol depletion can transform normal biconcave RBC into stomatocytes whereas anionic amphipaths, high salt, high pH, adenosine triphosphate (ATP) depletion, cholesterol enrichment, and proximity to a glass surface can transform normal biconcave RBC into echinocytes [12, 20]. These shape changes are reversible to the stage where sphero-stomatocyte and sphero-echinocyte become smooth spheres when small interior buds and vesicles are pinched off from the RBC surface [17]. These reversible RBC shape changes from biconcave shape to-and-from stomatocyte and echinocyte shapes are widely known as stomatocyte-discocyte-echinocyte (SDE) shape transformations. SDE shape transformations have a universal nature for the resultant shape and do not depend on the engaged shape-transforming agent [12].

Sheetz and Singer [21] proposed the widely known bilayer couple hypothesis to explain SDE transformation, and according to the bilayer-couple hypothesis, the two leaflets of the membrane bilayer responds differently to various perturbations and remain coupled to each other. Therefore, the expansion of the outer bilayer-leaflet relative to the inner bilayer-leaflet due to any shape-transforming agent results in convex forms on the membrane surface and induces echinocytes. Similarly, the expansion of the inner bilayer-leaflet relative to the outer bilayer-leaflet due to any shape-transforming agent results in concave forms on the membrane surface and induces stomatocytes. In this manner, the universal nature of SDE transformation is explained through the bilayer-couple hypothesis, and any change in relaxed area-difference between bilayer-leaflets is the necessary and sufficient factor for shape changes.

Several research studies have studied the SDE transformation [12, 13, 15, 17, 20, 22–34], and here, we discussed the development of an improved computational approach to accurately

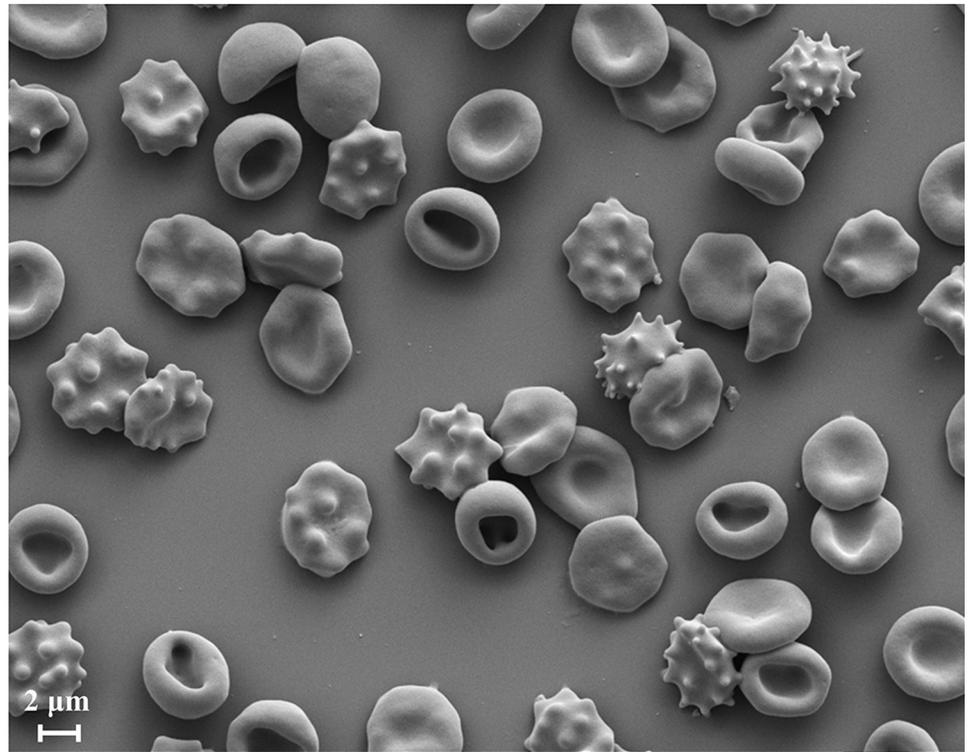


Fig 1. Scanning electron microscope (SEM) image of a RBC population having different morphology stages of stomatocytosis and echinocytosis.

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predict SDE transformation. Following subsections briefly introduce the computational approaches on RBC simulations in general, the bending energy models for SDE prediction, and discuss the few computational simulations on SDE transformation.

Computational simulations of RBC

Computational modelling and experimental studies have been carried out to investigate the bio-mechanical and rheological behaviour of RBC [9, 35–40]. Due to the simplicity of the RBC structure, they can be numerically approximated as a bag of concentrated haemoglobin solution surrounded by a thin macroscopically homogeneous membrane [13]. The thickness of the lipid bilayer being ~ 4 nm [28] and the offset between lipid bilayer-cytoskeleton being ~ 30 – 40 nm [28], RBC membrane can be treated as a two-dimensional (2D) viscoelastic surface in a three-dimensional (3D) space in the cellular length scale [9, 13]. The heterogeneous nature of the RBC membrane can be reasonably approximated as homogeneous in its properties for length scales above 100 nm [13, 41], and is suitable for mesoscopic and macroscopic scale investigations. However, a more realistic and accurate RBC representation requires detailed description of its structure, and therefore the incorporation of the properties of lipid bilayer, cytoskeleton and transmembrane proteins. There are several types of computational modelling and simulation approaches for RBC studies, and the prime approaches are continuum, particle-based and hybrid continuum-particle [41] based techniques. RBC membrane and associated fluid components are considered as homogeneous material under continuum approach, whereas the particle-based modelling represents these components via a network of springs and particulate assembly [42], respectively. It is difficult for the continuum approaches to incorporate the

detailed structure of RBC membrane, whereas particle-based methods are capable of detailed representation of the RBC membrane but require high computational cost to represent it at the molecular level through molecular dynamics approaches. Therefore, particle-based modelling approach in macroscale and mesoscale are widely used to study RBC behaviour. Besides, hybrid continuum-particle technique is the merging between continuum and particle-based approaches and can lead to more accurate and computationally efficient numerical simulations to study a broad range of biochemical and rheological behaviour of RBC.

For computational simulation purposes, the equilibrium RBC shape was derived by minimizing the in-plane shear energy and the out-of-plane bending energy under the reference constraints of cell membrane area and cell volume [9, 42]. There are several forms of Helfrich energy; spontaneous curvature model (SCM), bilayer coupling model (BCM), and area-difference-elasticity (ADE), which have been used to describe the RBC membrane bending energy [9, 23]. The SCM describes the membrane bending energy ($E_{Bending}^{SCM}$) for a membrane with surface area, A and local bending modulus, κ , such that [23, 24];

$$E_{Bending}^{SCM} [C_1, C_2] = \frac{\kappa}{2} \oint dA (C_1(r) + C_2(r) - \bar{C}_0)^2 \tag{1}$$

where, $C_1(r)$ and $C_2(r)$ are the principal curvatures at the point r on the membrane surface, and \bar{C}_0 is the spontaneous curvature. \bar{C}_0 indicates any asymmetry between the two bilayer-leaflets. The SCM model derived, vesicle shape is obtained at the minimum of $E_{Bending}^{SCM}$ for given A and vesicle volume, V .

The BCM is based on the bilayer-couple hypothesis, and assumes fixed area for a membrane lipid molecule and no molecular exchange between the two bilayer-leaflets. Therefore, the area of each bilayer-leaflet remains constant, and the area-difference between the two bilayer-leaflets (ΔA) can be determined from the integrated mean curvature over the membrane surface, such that [23];

$$\Delta A = D \oint dA (C_1(r) + C_2(r)) \tag{2}$$

where, D is the distance between bilayer leaflets. The membrane bending energy $E_{Bending}^{BCM}$ in this instance is determined for a defined reference surface with fixed ΔA as another constraint, such that [23];

$$E_{Bending}^{BCM} [C_1, C_2] = \frac{\kappa}{2} \oint dA (C_1(r) + C_2(r))^2 \tag{3}$$

The BCM model derived vesicle shape is obtained at minimum $E_{Bending}^{BCM}$ for given A , V and ΔA . It has been proven elsewhere [24, 27, 43] that both SCM and BCM models lead to same shape equations, and the vesicle shape behaviour is an extensively studied aspect [13, 15, 19, 23, 24, 27, 28, 31, 33, 34, 43–49]. The ADE model is a combined representation of SCM and BCM, and the ADE model determined membrane energy (E_{ADE}) for a vesicle having A , V and ΔA is as follows [23],

$$E_{ADE} [C_1, C_2, \Delta A] = \frac{\kappa}{2} \oint dA (C_1(r) + C_2(r) - \bar{C}_0)^2 + \frac{\bar{\kappa}}{2} \frac{\pi}{A D^2} (\Delta A - \Delta A_0)^2 \tag{4}$$

where, $\bar{\kappa}$ is the non-local bending modulus and ΔA_0 is the reference area-difference between bilayer-leaflets. The ADE model converges to SCM model at $\bar{\kappa}/\kappa \rightarrow 0$, and into BCM at $\bar{\kappa}/\kappa \rightarrow \infty$ [23, 46, 48]. The discocyte RBC shape is usually derived from SCM approach at

$\bar{C}_0 \sim 0$ [50], and the following approaches have been followed to predict the SDE transformation.

Computational simulations of SDE transformation

The shape, behaviour and deformability of a RBC have been extensively studied through computational simulation methods [9, 35, 36] for various conditions and scenarios. However, despite the numerous experimental and theoretical investigations on RBC shape transformations, the numerical predictions on full SDE transformations of RBC are limited [15, 47]. The existing limited number of numerical shape predictions use ADE membrane bending model to represent the bending resistance of the lipid-bilayer, and no information of the use of SCM and BCM in numerical implementations of SDE shape predictions are available. Nevertheless, the coarse-grained (CG)-RBC membrane model is developed on BCM approach and demonstrates the potential of BCM approach to accurately predict SDE transformation.

The studies by Lim et al. [19, 28, 49], and Khairy and Howard [31, 33] have used a continuum numerical approach based on ADE model to predict different stages of stomatocytes and echinocytes of SDE transformations. These studies have used a single parameter; effective-spontaneous-curvature as the control parameter to predict the different stages of SDE transformation under the constraints of membrane surface area and cell volume. The effective-spontaneous-curvature is a combination of both spontaneous membrane curvature and the reference area-difference of bilayer-leaflets, and at different values of effective-spontaneous-curvature, the corresponding RBC shape has been determined. It has also been identified that the effects of both spontaneous membrane curvature and bilayer-leaflet-area-difference are present in RBC membrane, and their effect is comparable in magnitude [19, 31]. Furthermore, any lipid asymmetry can be cancelled out by manipulating the bilayer-leaflet-area-difference, while any bilayer-leaflet-area-difference can be cancelled out by manipulating the lipid asymmetry of the lipid bilayer. Therefore, the spontaneous membrane curvature and the area-difference of bilayer-leaflets can be combined, and since, the spontaneous membrane curvature and the bilayer-leaflet-area-difference cannot yet be measured directly, it is also convenient to employ their combined effect through a single control parameter. However, the use of κ and $\bar{\kappa}$ in the same scale could lead to a significant difference [11] between the reference spontaneous membrane curvature and bilayer-leaflet-area-difference with the instantaneous membrane curvature and bilayer-leaflet-area-difference at the equilibrium. Furthermore, a detailed RBC membrane representation is required to study RBC shape transformations in the presence of membrane inhomogeneity, defective cytoskeleton and blood disorders that affect the membrane structure [8] such as hereditary-spherocytosis (HS) and hereditary-elliptocytosis (HE) [51, 52]. Therefore, the studies by Lim et al. [19, 28, 49], and Khairy and Howard [31, 33] are difficult to be extended to study the RBC morphology at above diseased conditions.

Chen and Boyle [15] have also developed a CG based spring-particle (SP) numerical approach to predict the SDE transformations, and have suggested a surface curvature approximation that is independent of the network topology to estimate the membrane bending energy. Their ADE model is comprised of the two distinct parameters; spontaneous membrane curvature and reference area-difference between bilayer-leaflets. However, the spontaneous membrane curvature and the reference area-difference between bilayer-leaflets, both being mathematical relationships of the membrane curvature, these control parameters for SDE transformation can be combined together as in the studies by Lim et al. [19, 28, 49], and Khairy and Howard [31, 33]. In addition, Chen and Boyle [15] have proposed shape boundaries for a wide range of RBC cell volume and membrane-area-difference. For all these SDE shape predictions; Lim et al. [19, 28, 49], Khairy and Howard [31, 33] and Chen and Boyle [15], the

minimum energy configuration of the RBC membrane has been determined by the in-plane elastic energy and out-of-plane bending energy, under the constraints on cell surface area and cell volume. Lim et al. [19, 28, 49], and Khiary and Howard [31, 33] have both employed the non-linear Skalak law to estimate the in-plane shear deformation of the RBC membrane. Chen and Boyle [15], in their CG approach, have adopted the worm-like-chain (WLC) type springs to estimate the resulting elastic energy between these CG particles. The membrane bending energy is estimated through discrete approximations of Helfrich's energy for membrane triangulation.

These computational simulation approaches qualitatively agree well with the experimental observations of RBC SDE transformation. However, all these studies have used the ADE model in which $\bar{\kappa}/\kappa \approx 1.0$, and the actual bilayer-leaflet-area-difference at the equilibrium differs from the reference conditions. Therefore, it is difficult to quantitatively compare numerical predictions against the experimental observations as the experimentally extracted bilayer-leaflet-area-difference is at the equilibrium. In addition, it is difficult to find any implementation of SCM method to successfully predict discocyte-echinocyte transformation. Therefore, it is reasonable to expect the presence of any bilayer-leaflet-area-difference with $\bar{\kappa}/\kappa \neq 1.0$ in order to predict discocyte-echinocyte transformation. Furthermore, if $\bar{\kappa}/\kappa \gg 1.0$ as in the case of BCM, then the deviation of the equilibrium bilayer-leaflet-area-difference from the reference conditions would be minimal. By this means, a framework to quantitatively validate the developed computational simulations against experimentally observed SDE transformation can be achieved, and will enhance the applicability of numerical predictions to investigate exact SDE transformation conditions. The universal nature of SDE transformation in the presence of echinocytic and stomatocytic shape-transforming agents can be adapted to suit distinctive scenarios if independent measurements of control parameters are available experimentally or computationally. Therefore, a CG-RBC membrane model inspired from the previous research by Lim et al. [19, 28, 49], is proposed with enhanced applicability to address some of the above concerns, namely, the significant difference between effective-spontaneous-curvature and instantaneous membrane curvature and bilayer-leaflet-area-difference at the equilibrium for ADE model, and the lack of framework to quantitatively validate the developed computational simulations against experimentally observed SDE transformation. The proposed improved CG-RBC membrane model predicts the SDE transformation and is first validated against experimentally observed RBC shapes. It is then applied to study the effect of reduced cell volume and elastic length scale on SDE transformation. Furthermore, the deformability of different stages of SDE transformation and the most probable cytoskeletal reference state of the RBC are investigated using the present CG-RBC membrane model.

Methods

The RBC membrane is the primary contributor for its mechanical nature since a RBC does not possess any internal structure. The lipid-bilayer contributes to its out-of-plane bending resistance and surface area incompressibility while the cytoskeletal spectrin network contributes to the in-plane shear deformation [53], and its cytoplasm contributes to the volume incompressibility of the RBC. The Helmholtz free energy of the RBC membrane is the collective contribution of out-of-plane membrane bending energy, in-plane shear energy and the energy penalty due to cell surface area and volume constraints relative to the specified reference membrane configuration. The equilibrium RBC shape is determined at the minimum free energy state of the RBC membrane.

Free energy of the CG-RBC membrane model

The developed CG-RBC membrane model employs N_v particles to represent the actin junctional complexes of the RBC membrane and form a 2D triangulated surface of N_t triangles. The N_s adjacent particle-particle connections of the triangulated surface represent the cytoskeletal spectrin links. The in-plane shear energy of the RBC membrane ($E_{Stretching}$) is estimated based on the coarse-graining approach implemented by Fedesov et al. [50], and is composed of an attractive potential (E_{WLC}) in the form of the WLC potential and a repulsive potential (E_{POW}) in the form of a power function. $E_{Stretching}$ can be expressed as follow [50];

$$E_{Stretching}(l_j) = \sum_{j \in 1 \dots N_s} [E_{WLC}(l_j) + E_{POW}(l_j)] \tag{5}$$

$$E_{WLC}(l_j) = \frac{k_B T l_{max}}{4 p} \frac{3x_j^2 - 2x_j^3}{1 - x_j} \tag{6}$$

$$E_{POW}(l_j) = \begin{cases} \frac{k_p}{(m - 1) l_j^{m-1}}, & m \neq 1 \\ -k_p \log(l_j), & m = 1 \end{cases} \tag{7}$$

where, l_j is the length of j^{th} link, k_B is the Boltzmann constant, T is the absolute temperature, l_{max} is the maximum link extension, p is the persistence length, k_p is the power function coefficient, and m is an exponent such that $m > 0$. x_j is defined as $x_j = l_j / l_{max}$. The experimentally estimated RBC membrane shear modulus (μ_0) lies between 4–12 μNm^{-1} [9, 50], and can be expressed as following for the CG-RBC membrane model [50]:

$$\mu_0 = \frac{\sqrt{3} k_B T}{4 p l_{max} x_0} \left(\frac{x_0}{2 (1 - x_0)^3} - \frac{1}{4 (1 - x_0)^2} + \frac{1}{4} \right) + \frac{\sqrt{3} k_p (m + 1)}{4 l_0^{m+1}} \tag{8}$$

where, l_0 is the equilibrium length of spectrin link and defined as $x_0 = l_0 / l_{max}$. The parameters k_p and p can be estimated for a given μ_0 and x_0 using Eqs (5) and (8) at the equilibrium state of specified cytoskeletal reference state.

The out-of-plane bending energy of the RBC membrane ($E_{Bending}$) is estimated based on a discrete approximation of the Helfrich energy model [54] for a zero spontaneous membrane curvature, such that:

$$E_{Bending} = 2 \kappa \sum_{j \in 1 \dots N_s} \frac{M_j^2}{\Delta A_j} \tag{9}$$

M_j is the membrane curvature at the triangle-pair that shares the j^{th} link, and ΔA_j represents the surface area associated with the j^{th} link. M_j and ΔA_j can be given as:

$$M_j = \frac{1}{2} l_j \theta_j \tag{10}$$

$$\Delta A_j = \frac{1}{3} (A_{T1} + A_{T2}) \tag{11}$$

where θ_j is the angle between outward normal vectors to the triangles sharing j^{th} link, and A_{T1} and A_{T2} are the planer area of T1 and T2 triangles respectively that share the j^{th} link. The

concave arrangement of a triangle-pair results in positive M_j , whereas the convex arrangement of a triangle-pair results in negative M_j . An illustration of the triangle-pair made of T1 and T2 triangles that shares the j^{th} link is provided in Fig 2.

The energy components due to RBC surface area constraint ($E_{\text{Surface Area}}$) and the cell volume constraint (E_{Volume}) are estimated as follows [50, 53]:

$$E_{\text{Surface Area}} = \frac{1}{2} k_A \left(\frac{A - A_0}{A_0} \right)^2 A_0 + \sum_{k \in 1 \dots N_t} \frac{1}{2} k_a \left(\frac{A_k - A_{k,0}}{A_{k,0}} \right)^2 A_{k,0} \tag{12}$$

$$E_{\text{Volume}} = \frac{1}{2} k_v \left(\frac{V - V_0}{V_0} \right)^2 V_0 \tag{13}$$

where, A_0 is the reference membrane surface area, A is the instantaneous membrane surface area, $A_{k,0}$ is the reference area of k^{th} triangle, A_k is the instantaneous area of k^{th} triangle, V_0 is the reference cell volume and V is the instantaneous cell volume. k_A , k_a and k_v represent the total surface area, local surface area and volume constraint coefficients, respectively. The resistance of the lipid-bilayer for surface area change is considered for both the whole RBC surface and for individual triangular element, as the lipid-bilayer is anchored to the cytoskeleton through transmembrane proteins and therefore, the movement of lipid molecules over the membrane is restricted [55]. The first part of Eq (12) represents the total surface area constraint whereas the second part of Eq (12) represents the triangular element surface area constraint.

A BCM-based membrane bending energy approach is implemented in the CG-RBC membrane model to predict SDE transformations. Therefore, in addition to above energy components, another two constraints are included to the system to maintain a reference area-difference between bilayer-leaflets and to maintain a reference total-membrane-curvature. The area-difference between bilayer-leaflets with D_0 monolayer thickness can be estimated based on a discrete approximation as follows [19, 49]:

$$\Delta A = 2 D_0 \sum_{j \in 1 \dots N_s} M_j \tag{14}$$

The energy penalty of the membrane due to the constraint to maintain reference bilayer-leaflet-area-difference ($E_{\text{Area-difference}}$) is considered to be proportional to the square of the

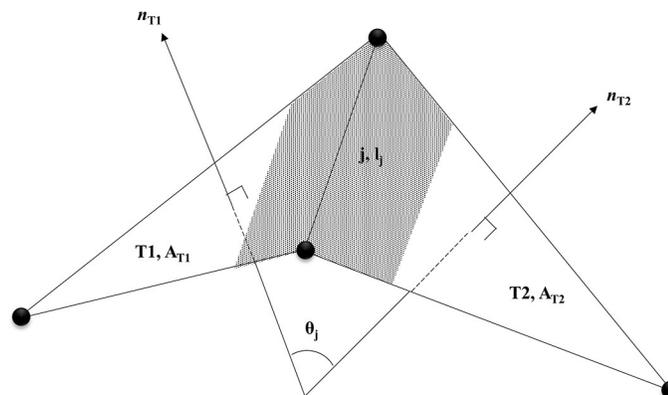


Fig 2. Illustration of M_j at j^{th} link. The shaded planer area is the area associated with the j^{th} link. n_{T1} and n_{T2} are the normal vectors to the triangles T1 and T2 respectively.

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difference between ΔA and the reference bilayer-leaflet-area-difference (ΔA_0), and can be given as follows:

$$E_{Area-difference} = \frac{1}{2} \frac{\pi k_{ad}}{D_o^2} \left(\frac{\Delta A - \Delta A_0}{A} \right)^2 A \tag{15}$$

where, k_{ad} is the bilayer-leaflet-area-difference constraint coefficient. Following-up on the discussion in section; ‘Computational simulations of RBC’, ADE model converges to BCM at $\bar{\kappa}/\kappa \rightarrow \infty$, and therefore, it is reasonable for k_{ad} to adopt a significantly higher value than κ . Furthermore, the comparison between Eqs (4) and (15) shows that $\bar{\kappa} \approx 4.0 k_{ad}$. In the ADE model, κ and $\bar{\kappa}$ are in the same order [19, 49], and therefore the competition between spontaneous membrane curvature and bilayer-leaflet-area-difference, leads to consistent RBC shapes as minimum energy configuration for specified reference conditions. However, for the BCM model, inconsistent RBC shapes can arise at similar ΔA_0 as $\bar{\kappa}$ is of higher order than κ , and therefore is the dominant component. ΔA is the integrated mean curvature over the membrane surface, and therefore ΔA_0 can be achieved at multitude combinations of direction-dependent mean curvature at any point on the membrane surface. Equivalently, in the case of present discrete approximation of ΔA , the reference ΔA_0 can be achieved at multitude convex and concave combinations of triangular-pair arrangement over the membrane surface. Therefore, to restrict the inconsistency of resultant RBC shape, the total-membrane-curvature constraint is introduced to the system. The total-membrane-curvature can be presented as the integrated direction-independent mean curvature over the membrane surface. Consequently, the minimum energy configuration of a RBC at specified ΔA_0 can be obtained at a consistent convex and concave combination of triangular-pair arrangement over the membrane surface, which is also in agreement with the specified reference total-membrane-curvature (C_0). The instantaneous total-membrane-curvature (C) for any RBC shape is higher than ΔA since it considers the absolute value of mean curvature over the membrane surface. C can be estimated as follows:

$$C = 2 D_o \sum_{j \in 1 \dots N_s} |M_j| \tag{16}$$

Therefore, the energy penalty of the membrane arising due to the constraint to maintain specified C_0 ($E_{Total-curvature}$) is defined as follows:

$$E_{Total-curvature} = \frac{1}{2} \frac{\pi k_C}{D_o^2} \left(\frac{C - C_0}{A} \right)^2 A \tag{17}$$

where k_C is the total-membrane-curvature constraint coefficient, and one can expect k_C to be within the same order of $\bar{\kappa}$. The total free energy of the membrane (E), can therefore be determined by the summation of all these energy components, such that:

$$E = E_{Stretching} + E_{Bending} + E_{Surface Area} + E_{Volume} + E_{Area-difference} + E_{Total-curvature} \tag{18}$$

It is assumed that the membrane particles move over the RBC membrane to achieve the minimum free energy state. The force (F_i) acting on the i^{th} membrane vertex point at the point r_i on the surface can be derived from the principle of virtual work, such that,

$$F_i = - \frac{\partial E}{\partial r_i}, i \in 1 \dots N_v \tag{19}$$

The motion of i^{th} point can be described from the Newton's second law of motion as follows:

$$F_i = m_i \ddot{r}_i + c \dot{r}_i \tag{20}$$

where, m_i is the mass of i^{th} particle, dot ($\dot{}$) is the time derivative and c is the viscosity of RBC membrane.

Model parameters for RBC shape prediction

The initial spherical geometry is built up on an icosahedron of equilateral triangular faces that is inscribed within a sphere [19, 49, 56] of radius R_{RBC} . R_{RBC} is determined for a sphere having equivalent surface area to a RBC. The physiological RBC surface area being $\sim 140 \mu\text{m}^2$ [2, 5], A_0 is selected as $140 \mu\text{m}^2$ and therefore the estimated $R_{\text{RBC}} = 3.34 \mu\text{m}$. The refinement of triangulation is obtained by generating new vertices at midpoints of each triangular face edge, and combining the vertices together such that the preceding triangular surface is divided into four smaller triangles. The new vertices are then projected radially onto the spherical surface with the radius R_{RBC} . The minimum required particle resolution is determined such that the percentage error (ϵ) for estimating $E_{\text{Stretching}}$, E_{Bending} , A , V and ΔA for the initial spherical geometry falls below 1.0% against the analytical estimations. The present CG-RBC membrane model consists of $N_v = 2,562$ membrane vertex points, $N_t = 5,120$ triangular elements and $N_s = 7,680$ adjacent particle-particle connections. The quality of the triangulation is determined by the distribution of adjacent particle-particle connection length and the distribution of adjacent particle-particle connection for each vertex point [50]. The former is attributed to the ratio of standard deviation of the adjacent particle-particle connection length to the average adjacent particle-particle connection length. A smaller value is preferred for this ratio, and for the present consideration the value of this ratio is only 0.065. It is also preferred to have a higher percentage of vertex points having 6 adjacent particle-particle connections. In the present CG-RBC membrane, only the 12 vertices (= 0.47%) on the initial icosahedron have 5 particle-particle connections, whereas all the remaining membrane vertex points (= 99.53%) have 6 particle-particle connections. Therefore, the CG-RBC membrane has high quality of triangulation, and the effects of inhomogeneity can be considered minimal during SDE transformation.

The reference state of the cytoskeleton is assumed as an ellipsoid at 0.94 of volume of a sphere having A_0 surface area, and the equilibrium length of the spectrin link l_0 is determined at this reference state. The membrane shear modulus, μ_0 is set at $4.0 \mu\text{Nm}^{-1}$ and agrees with the physiological shear modulus [9, 50], whereas the parameters k_p , p and l_{max} are estimated at the room temperature, $T = 296.15 \text{ K}$, and at $m = 2$ and $x_0 = 0.45$ [50].

The experimentally estimated RBC membrane bending modulus lies in the range of 1×10^{-19} – $7 \times 10^{-19} \text{ Nm}$ [9, 57], and therefore κ is selected to be $2.5 \times 10^{-19} \text{ Nm}$. The constraint coefficients k_A , k_a , k_v , k_{ad} and k_C are set to $1 \times 10^{-3} \text{ Nm}^{-1}$, $5 \times 10^{-5} \text{ Nm}^{-1}$, 100 Nm^{-2} , $7.5 \times 10^{-17} \text{ Nm}$ and $2.5 \times 10^{-17} \text{ Nm}$, respectively to achieve reference constraint conditions. The reference triangular element surface area ($A_{k,0}$) is set at the corresponding triangular element area at cytoskeletal reference state. The reference cell volume (V_0) is considered as $93.48 \mu\text{m}^3$ in agreement with the physiological RBC volume [2, 5], and is 0.6 of volume of the sphere of radius R_{RBC} . The lipid monolayer thickness (D_0) is considered as 2 nm. $\Delta A_0/A_0$ and C_0/A_0 are set within the ranges of 0.05% - 0.30% and 0.30% - 0.90% respectively to predict different stages of SDE transformation.

The motion of RBC membrane particles to reach the equilibrium state, is estimated at $c = 1 \times 10^{-7} \text{ Nsm}^{-1}$ and $m_i = 1 \times 10^{-9} \text{ kg}$. The parameters c and m_i do not affect the equilibrium RBC shape as they only control the speed of achieving the equilibrium state [54]. The updated

velocity (\dot{r}_i) and the position (r_i) of the i^{th} vertex at time ($t + \Delta t$) from time (t) is given as follows;

$$\dot{r}_i(t + \Delta t) = c \dot{r}_i(t) + \ddot{r}_i(t) \Delta t \tag{21}$$

$$r_i(t + \Delta t) = r_i(t) + \dot{r}_i(t + \Delta t) \Delta t \tag{22}$$

where, Δt is the time-step for succeeding iteration. The iterations are continued until the RBC membrane reaches the equilibrium state, which is the minimum free energy state of the RBC membrane at given reference conditions. In the present computational implementation of CG-RBC membrane model, the equilibrium cell state is acknowledged when the change between each analogous energy component ($E_{\text{Stretching}}$, E_{Bending} , $E_{\text{Surface Area}}$, E_{Volume} , $E_{\text{Area-difference}}$, $E_{\text{Total-curvature}}$) at two successive iterations, is less than 1×10^{-7} in the order of energy component in consideration.

Validation of CG-RBC membrane model

Qualitative validation of CG-RBC membrane model predicted SDE transformation.

RBC SDE shape transformation is predicted at reference reduced cell volume (v) and fitting combinations of ΔA_0 and C_0 conditions. v specifies the cell volume relative to the sphere having equivalent cell surface area, and is defined as follows:

$$v = \frac{V_0}{4/3 \pi R_{RBC}^3} \tag{23}$$

Several shape classes can be observed as the minimum energy configuration at combinations of different v , ΔA_0 and C_0 . The SDE shape transformation presented in Fig 3 is predicted at $v = 0.6$, $0.05\% \leq \Delta A_0/A_0 \leq 0.30\%$ and $0.30\% \leq C_0/A_0 \leq 0.90\%$, and is compared with both experimental observations and different numerical predictions. Experimental observations from SEM imaging (refer to S1 Appendix for detailed information. The laboratory protocol is available at <http://dx.doi.org/10.17504/protocols.io.yvhfw36>), and the numerical predictions by Lim et al. [19, 28, 49] and Chen and Boyle [15] are used for the comparison in Fig 3. It can be observed that the predicted SDE transformation through the implemented CG-RBC membrane model agrees well with the experimentally observed and numerically predicted results. The implemented CG-RBC model is also capable of predicting the sphero-stomatocyte (stomatocyte IV) and sphero-echinocyte (echinocyte IV) stages as stable minimum energy configurations, which have not been predicted by other numerical approaches. The predicted sphero-stomatocyte shape consists with small interior buds that are attached to the membrane surface whereas the sphero-echinocyte shape consists of small sharp projections as expected. Therefore, the CG-RBC membrane model can predict the complete SDE transformation at constant cell surface area and cell volume constraints.

Quantitative validation of CG-RBC membrane model predicted SDE transformation.

In addition to the qualitative validation presented in Fig 3, a quantitative analysis is performed on the predicted RBC shapes obtained using the CG-RBC membrane model against experimental data extracted from 3D confocal microscopy imaging of RBC. Different shapes were obtained by changing buffer composition before labelling and fixing the cells (refer to S2 Appendix for detailed information. The laboratory protocol is available at <http://dx.doi.org/10.17504/protocols.io.yjyfupw>). Imaging data were then analysed using numerical methods to recreate a triangulated mesh over the surface of the cells. Experimental measurements were calibrated using fluorescent beads with a known diameter and imaged at the same time as the RBC. Calibration enabled accurate measurements of RBC surface area and volume.

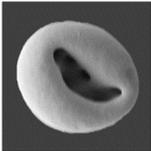
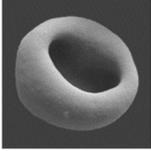
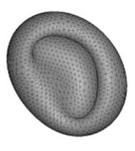
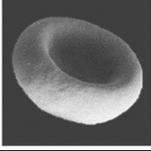
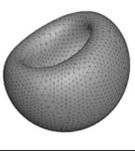
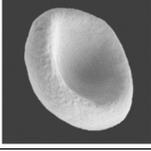
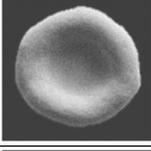
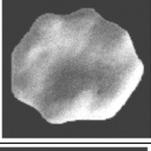
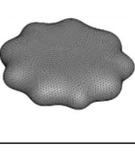
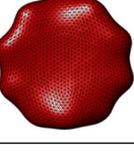
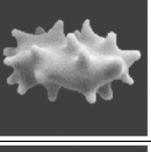
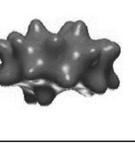
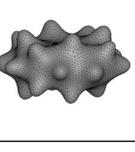
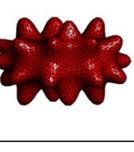
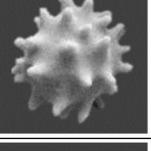
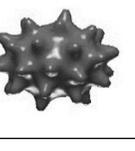
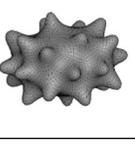
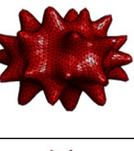
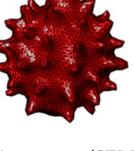
Shape Classification		Experimental Observations (SEM Imaging)	Numerical Predictions					
			Continuum	SP-RBC	CG-RBC			
					v	$\Delta A_0/A_0$ (%)	(C_0/A_0) (%)	Predicted Shape
Stomatocyte	IV				0.60	0.050	0.300	
	III				0.60	0.100	0.195	
	II				0.60	0.105	0.175	
	I				0.60	0.115	0.165	
Discocyte					0.60	0.120	0.185	
Echinocyte	I				0.60	0.135	0.200	
	II				0.60	0.190	0.550	
	III				0.60	0.225	0.600	
	IV				0.60	0.300	0.900	

Fig 3. Comparison of SDE shape transformation predicted using CG-RBC membrane model with scanning electron microscopy (SEM) experimental observations and different numerical prediction techniques. The corresponding CG-RBC membrane model parameters of reference reduced cell volume (v), bilayer-leaflet-area-difference (ΔA_0) and total-membrane-curvature (C_0) are indicated next to the

predicted RBC shape. Representative images for the shapes predicted by Lim et al. [19, 28, 49] through continuum approach (G. H. W. Lim, personal communication, March 19, 2019), and by Chen and Boyle [15] through SP-RBC model (M. Chen, personal communication, September 13, 2018) are presented. These images are similar but not identical to the original images from Lim et al. [19, 28, 49] and Chen and Boyle [15], and therefore for illustrative purposes only.

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The cell surface area (A^{ex}), cell volume (V^{ex}), bilayer-leaflet-area-difference (ΔA^{ex}) and total-membrane-curvature (C^{ex}) are estimated from these generated triangulated surfaces for four randomly selected RBC having discocyte, echinocyte I, echinocyte II and echinocyte III shapes, and are summarized in Fig 4. The estimated $\Delta A^{ex}/A^{ex}$ and C^{ex}/A^{ex} for these experimentally obtained RBC are introduced to the CG-RBC membrane model as reference $\Delta A_0/A_0$ and C_0/A_0 parameters, and the resultant shape is determined at equivalent reduced cell volume (v^{ex}) constraint. v^{ex} for the randomly selected RBC each having discocyte, echinocyte I, echinocyte II and echinocyte III shapes, is defined according to Eq (24).

$$v^{ex} = \frac{V^{ex}}{\text{Volume of a sphere having equivalent } A^{ex}} \tag{24}$$

Assuming rigid body conditions, the centre of mass of the whole cell and its three-principle axes of inertia are determined for each experimentally observed and numerically predicted cell shapes. H_1 , H_2 and H_3 are defined as the distance between the furthest vertex points on RBC membrane surface along these three-principle axis of inertias of the cell such that $H_1 \leq H_2 \leq H_3$, and used to estimate the cellular measurements: the normalized cell length

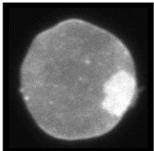
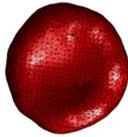
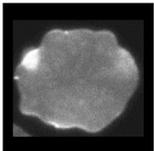
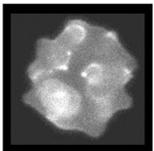
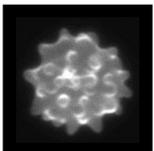
Shape Classification	Experimental Observations (Confocal Microscopy Imaging)	Experimental Observations (Triangulated Surface Mesh)	A^{ex} (μm^2)	V^{ex} (μm^3)	$\Delta A^{ex}/A^{ex}$ (%)	C^{ex}/A^{ex} (%)	v^{ex}
Discocyte			145.046	101.623	0.124	0.244	0.619
Echinocyte	I		129.634	82.052	0.138	0.298	0.591
	II		140.054	91.767	0.143	0.411	0.589
	III		131.450	91.547	0.161	0.624	0.646

Fig 4. Summary of estimated cell surface area (A^{ex}), cell volume (V^{ex}), bilayer-leaflet-area-difference (ΔA^{ex}), total-membrane-curvature (C^{ex}) and equivalent reduced cell volume (v^{ex}) for the experimentally observed discocyte, echinocyte I, echinocyte II and echinocyte III RBC shapes.

<https://doi.org/10.1371/journal.pone.0215447.g004>

(H_x), normalized cell thickness (H_z) and shape factor (SF). H_x is defined as the ratio between H_3 and the equivalent spherical radius (R^*), where R^* is the radius of the sphere having equivalent cell surface area. Similarly, H_z is defined as the ratio between H_1 and R^* . $SF = H_1 / \sqrt{H_2 \times H_3}$ [58], and indicates the sphericity of the cell. The cell becomes more and more spherical as SF reaches the value 1, and becomes more and more flattened disc as SF reaches 0.

These three cellular measurements are used to quantitatively compare the corresponding experimentally observed and numerically predicted RBC shapes. The estimated percentage error values (ϵ) for H_x , H_z and SF between corresponding experimentally observed and numerically predicted RBC shapes are presented in Fig 5. It can be observed that the resulting shapes obtained through CG-RBC membrane model agree well with the shapes derived from 3D confocal microscopy imaging. The values of ϵ for H_x , H_z and SF are reasonable and the maximum ϵ (= 21.65%) is for the H_z in the case of echinocyte III RBC shape. However, any experiment error during 3D confocal microscopy imaging and image analysis can lead to ϵ while triangulated surface generation can also be another contributing factor. Therefore, the resulting ϵ is the resultant effect of any experimental errors, any triangulated surface generating errors and any error in CG-RBC shape predictions. It can be observed that ϵ is generally higher for H_z than H_x , which contributes to ϵ for SF as well. The experimentally observed cell being not completely lying on the bottom surface of the imaging chamber leads to over prediction of H_z . Therefore, better fixation of the cell during 3D confocal imaging experiments can improve the accuracy of H_z measurements. In addition, the accuracy of $\Delta A^{ex}/A^{ex}$ and C^{ex}/A^{ex} estimations can be improved by generating a more homogeneous triangular network having similar triangular edge lengths. By this means, it is possible to improve the accuracy of

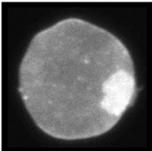
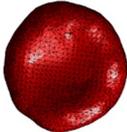
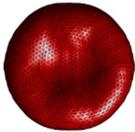
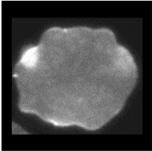
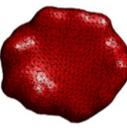
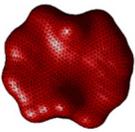
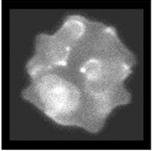
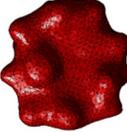
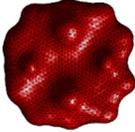
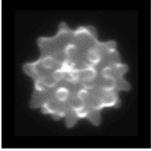
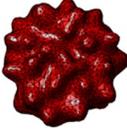
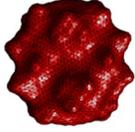
Shape Classification		Experimental Observations (Confocal Microscopy Imaging)	Experimental Observations (Triangulated Surface Mesh)	CG-RBC Membrane Model Prediction	ϵ (%)		
					H_x	H_z	SF
Discocyte					2.74	13.41	12.56
Echinocyte	I				2.00	18.90	16.18
	II				10.29	11.95	2.88
	III				5.45	21.65	16.18

Fig 5. Summary of estimated percentage error (ϵ) for normalized cell length (H_x), normalized cell thickness (H_z) and shape factor (SF) between corresponding experimentally observed and CG-RBC membrane model predicted RBC shapes.

<https://doi.org/10.1371/journal.pone.0215447.g005>

experimentally derived measurements, which can improve the comparability between analogous experimental observations and numerical predictions. However, the maximum ϵ being 21.65%, is acceptable based on all these uncertainties, and therefore the CG-RBC model is capable of quantitatively represent different SDE morphologies.

Results and discussion

Effect of RBC reduced volume on SDE transformation

The CG-RBC membrane model is used to investigate the effect of reduced cell volume (v) on SDE transformation. In an isotonic environment, v is equivalent to 0.6 whereas v increases or decreases in hypotonic and hypertonic environments, respectively. The insight on SDE behaviour at different tonicity conditions facilitate the better understanding of SDE behaviour at specific shape-transforming conditions. Therefore, RBC shapes are predicted at similar reference conditions of ΔA_0 and C_0 as presented in Fig 3 and at different v condition ($v = 0.55, 0.60, 0.65, 0.70$ and 0.75). The stable minimum energy configurations at specified ΔA_0 , C_0 and v are illustrated in Fig 6 for stomatocyte II, discocyte and echinocyte II stages. The BCM model can predict stable vesicle shapes if the ratio of $\bar{\kappa}/\kappa$ is above the critical value at v [23, 48], and for the present consideration, $\bar{\kappa}/\kappa = 150$, a value well above the critical ratio of $\bar{\kappa}/\kappa = (0, 20)$ for $v = [0.55, 0.75]$.

It can be observed that the predicted RBC shapes become more spherical as expected with the increase in v . H_x for the SDE transformation gradually reduces whereas H_z increases, and therefore the SF also increases gradually with the increase in v . The membrane curvature corresponding to i^{th} membrane vertex point ($C_{v,i}$) is defined as follows:

$$C_{v,i} = \sum_{jj \in 1 \dots N_{s,i}} \frac{M_{jj}}{\Delta A_{jj}} \tag{25}$$

where, $N_{s,i}$ is the number of associated spectrin links with the i^{th} membrane vertex point, and

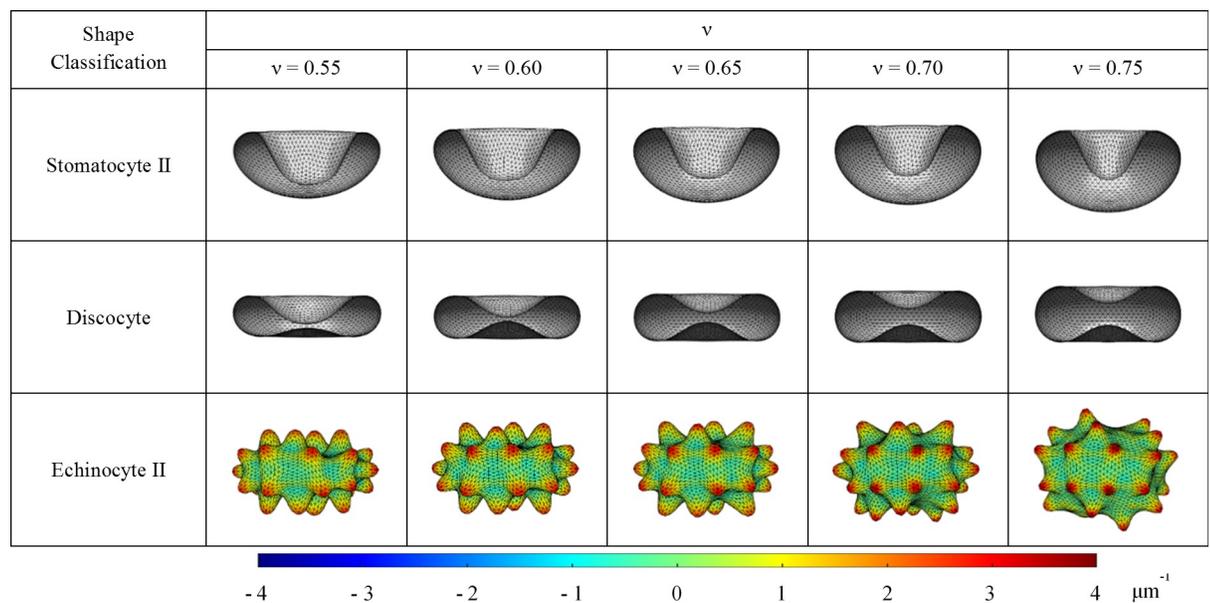


Fig 6. CG-RBC membrane model predicted stomatocyte II, discocyte and echinocyte II shapes at reduced cell volumes of $v = 0.55, 0.60, 0.65, 0.70$ and 0.75 . The coloured regions of the echinocyte II shape represent the membrane curvature on its' vertex points ($C_{v,i}$).

<https://doi.org/10.1371/journal.pone.0215447.g006>

M_{jj} and ΔA_{jj} represent the membrane curvature at the triangle-pair that shares the jj^{th} spectrin link and the surface area associated with it, respectively. It can also be observed (refer to Fig 6) that the maximum $C_{v,i}$ for echinocyte II, echinocyte III and echinocyte IV shapes increase rapidly whereas the minimum $C_{v,i}$ for stomatocyte II, stomatocyte III and stomatocyte IV decrease with increase in v . Therefore, it can be summarized that the absolute $C_{v,i}$ for stomatocyte II, III and IV stages and echinocyte II, III and IV stages increases rapidly with the increase in v whereas no significant change can be observed for stomatocyte I, discocyte and echinocyte I shapes. In general, for the stomatocyte shape, the oval shaped concavity mouth becomes more circular and its minimum cell thickness increases with v . Similarly, the predicted discocyte shape shows asymmetric biconcavity at low v , which becomes more symmetric with increasing v . The minimum cell thickness of discocyte also increases with v . For the echinocyte shapes, the spicules become narrower and sharper with uneven distribution over the membrane surface with the increase of v . Therefore, the outcomes of the study on the effect of v on SDE transformation suggest that though the predicted SDE shape class has not been affected by the changes in v , the features of the resultant RBC shape is affected. Therefore, the SDE transformations with equivalent reference conditions of ΔA_0 and C_0 behave differently at different v conditions, and one should consider all the relevant reference conditions to accurately predict the resultant RBC morphology.

Effect of RBC elastic length scale on SDE transformation

It has been found that the RBC membrane bending modulus differs for different SDE morphology [59], whereas the RBC membrane stiffness increases with in-vitro cell ageing and several diseased conditions such as malaria infection, SCA, HS and HE [9]. Therefore, the CG-RBC membrane model is used to investigate the effect of elastic length scale (Λ_{el}) on SDE transformation. Λ_{el} is the relation of RBC membrane bending modulus (κ) to its shear modulus (μ_0), and is defined as follows [13]:

$$\Lambda_{el} = \sqrt{\frac{\kappa}{\mu_0}} \tag{26}$$

Li et al. [60] have suggested that the Λ_{el} should be above a critical value ($\sim 0.37 \mu\text{m}$) at the spherical cytoskeletal reference state in order to obtain the discocyte shape as the possible minimum free energy configuration. Otherwise, stomatocyte shape is resulted as the minimum free energy configuration. However, Mukhopadhyay et al. [13] have used $\Lambda_{el} = 0.28 \mu\text{m}$ at zero prestressed cytoskeletal reference state, whereas Lim et al. [19, 49] have used $\Lambda_{el} = 0.28 \mu\text{m}$ at the ellipsoidal cytoskeletal reference state, in order to investigate RBC shapes and shape transformations. Moreover, Tsubota [54] has investigated the critical value of Λ_{el} at the shape transition between stomatocyte and discocyte for several forms of out-of-plane bending energy estimations. In the present study, SDE transformation presented in Fig 3 is obtained at $\Lambda_{el} = 0.25 \mu\text{m}$ at an ellipsoidal cytoskeletal reference state, and agrees with the critical limits of Λ_{el} suggested by Tsubota [54] for the corresponding out-of-plane bending energy form.

Several Λ_{el} [$\Lambda_{el} (\mu\text{m}) = 0.11, 0.18, 0.25, 0.35$ and 0.56] values are achieved at 5.0, 2.0, 1.0, 0.5 and 0.2 multiplications of μ_0 ($\mu_0 = 4.0 \mu\text{Nm}^{-1}$) at constant κ ($\kappa = 2.5 \times 10^{-19} \text{Nm}$), where μ_0 and κ are in the physiological range for cytoskeletal shear modulus and membrane bending modulus. RBC shapes are predicted at similar reference conditions of ΔA_0 , C_0 , and v as presented in Fig 3 but at varying Λ_{el} . The behaviour of SDE transformation at varying Λ_{el} is illustrated in Fig 7 for stomatocyte II, discocyte and echinocyte II stages, which each represents the stomatocyte, discocyte and echinocyte stages, respectively. The cellular measurements; H_x , H_z

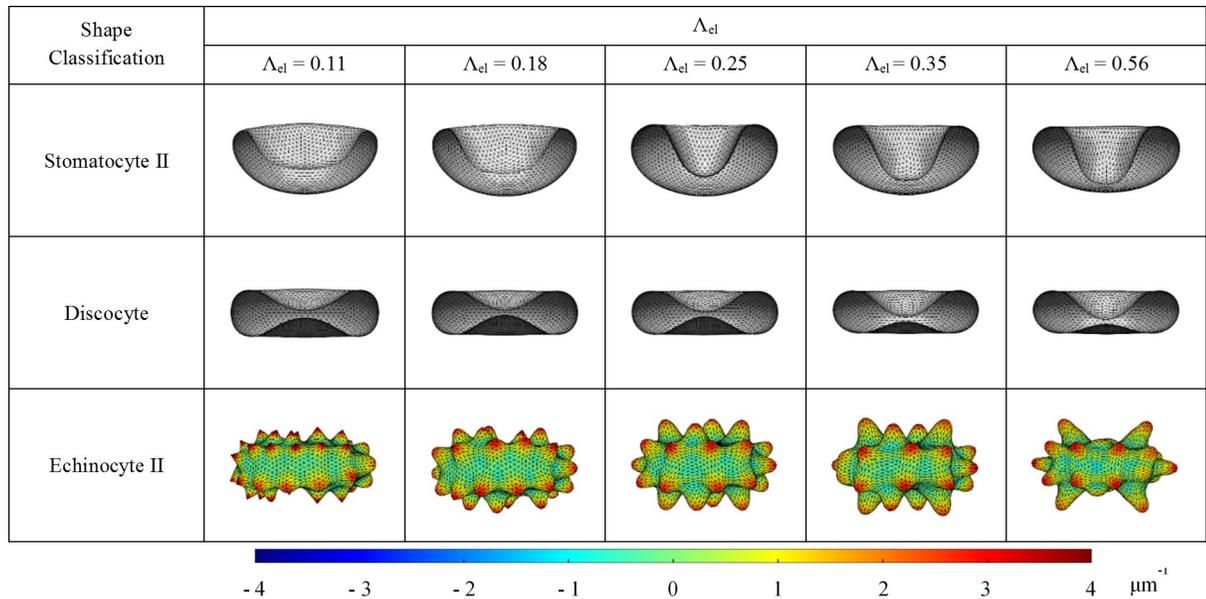


Fig 7. CG-RBC membrane model predicted stomatocyte II, discocyte and echinocyte II shapes at varying elastic length scale, $\Lambda_{el} = 0.11, 0.18, 0.25, 0.35$ and 0.56 . The coloured regions of the echinocyte II shape represent the membrane curvature on its' vertex points ($C_{v,i}$).

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and SF do not show significant variation with the change in Λ_{el} . However, the maximum $C_{v,i}$ for echinocyte II, echinocyte III and echinocyte IV shapes decreases rapidly whereas the minimum $C_{v,i}$ for stomatocyte II, stomatocyte III and stomatocyte IV increases with the increase in Λ_{el} . Therefore, it can be summarized that the absolute $C_{v,i}$ for stomatocyte II, III and IV stages and echinocyte II, III and IV stages decreases rapidly with the increase in Λ_{el} whereas no significant change can be observed for stomatocyte I, discocyte and echinocyte I shapes. In general, for the stomatocyte shape, the oval shaped concavity mouth becomes more circular and its minimum cell thickness decreases with Λ_{el} . Similarly, the predicted discocyte shape shows asymmetric biconcavity at high Λ_{el} while the more symmetric biconcavity becomes less symmetric with increasing Λ_{el} . However, the minimum cell thickness of discocyte does not indicate significant change with Λ_{el} . For the echinocyte shapes, the spicules become broader and the spicule size become irregular with the increase of Λ_{el} . At lower Λ_{el} values, the contribution from membrane bending energy component becomes less significant and therefore result in higher values of absolute $C_{v,i}$ for equilibrium RBC shapes. On the contrary, the membrane bending energy becomes more dominant at higher Λ_{el} values and restricts $C_{v,i}$ for equilibrium RBC shapes. Therefore, smoother RBC membrane can be observed and it becomes difficult for equilibrium RBC shapes to reach the exact reference area-difference between bilayer-leaflets and total-membrane-surface-curvature conditions at higher Λ_{el} values. These results reveal how the features of SDE transformation have been affected by the changes in Λ_{el} , and therefore provide valuable insight to SDE behaviour at different shape-transforming scenarios.

Deformability of SDE transformation

The RBC membrane elasticity is a critical physiological index [61], and a RBC needs high elasticity to carry out its function as a gas carrier in the microcirculation. The main contributors of RBC deformability are cell geometry, intra-cellular and extra-cellular fluid viscosity and elastic properties of the cell membrane [62, 63]. Therefore, any change in cell deformability

can be attributed to the change in one or more of these contributors. The highly deformable discocyte shape becomes more and more stiffer and finally rigid when it follows different stages through discocyte-spherocyte [64]. This phenomenon can be linked with the evolution of SF during SDE transformation, and Fig 8 summarises the estimated SF for the CG-RBC membrane model predicted SDE transformation stages that are presented in Fig 3. SF for the discocyte shape is the lowest, and increases progressively with stages I, II and III of stomatocytosis and echinocytosis where it reaches the maximum SF for sphero-stomatocyte and sphero-echinocyte shapes. The evolution of SF values can therefore be used as an indicator of RBC deformability during SDE transformation, and as such, the CG-RBC model has a strong potential in accurately predicting RBC deformability at different SDE stages.

Furthermore, the SDE transformation due to stomatocytic and echinocytic shape-transforming agents take place at constant membrane surface area and cell volume [11–16], and equivalently the CG-RBC membrane model predicted SDE transformation follows at constant reduced cell volume ($v = 0.6$) (refer to Fig 3). Therefore, intra-cellular and extra-cellular fluid viscosity and/ or elastic properties of the cell membrane are the most likely deformability factors to be affected during reversible SDE transformation.

Cytoskeletal reference state of RBC

The stress-free reference state of the cytoskeleton is a controversial subject [4, 42]. Several studies [4, 60] have suggested that a significantly lower cytoskeletal elasticity is needed to achieve a biconcave shape for a spherical cytoskeletal reference state. Otherwise, a non-spherical reference state; biconcave or ellipsoidal cytoskeletal reference states, must be assumed to achieve stable biconcave shape at physiological cytoskeletal elasticity. Lim et al. [19, 28, 49] numerically proposed that the cytoskeletal reference state of the RBC is most likely to be an ellipsoid with a reduced volume in the range of 0.925–0.976 of a sphere having equivalent

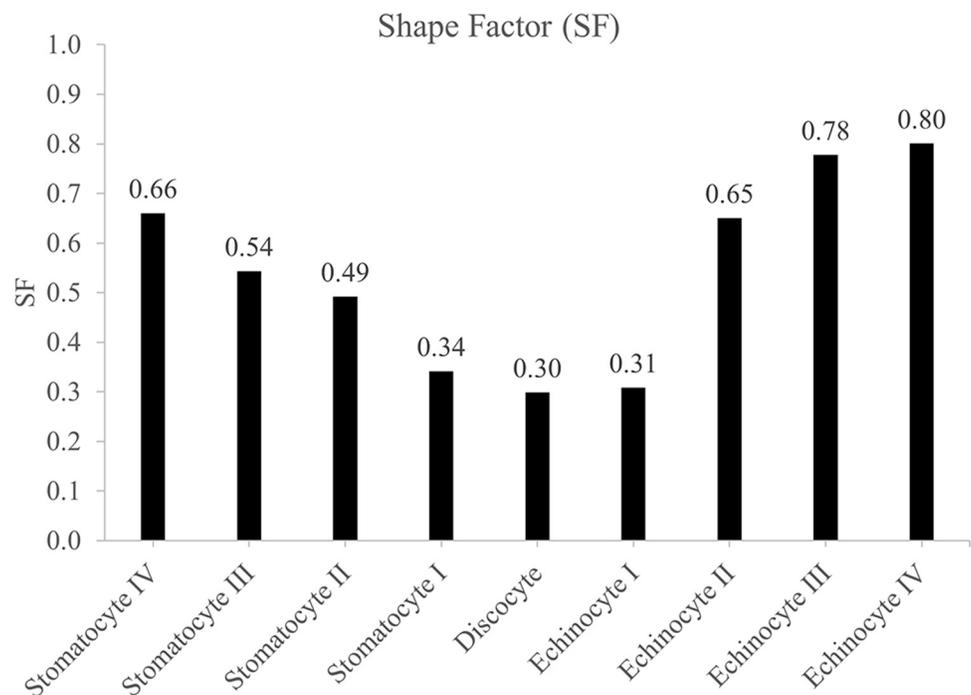


Fig 8. Shape Factor (SF) for CG-RBC membrane model predicted stomatocyte IV—echinocyte IV RBC shapes.

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surface area, and Khairy and Howard [31] have also suggested that the cytoskeletal reference state is most likely to be an ellipsoidal shape.

The investigation for the cytoskeletal reference state is carried out also with the implemented CG-RBC membrane model. The equilibrium spectrin length, l_0 is extracted at several cytoskeletal reference states, and used in CG-RBC membrane model to predict discocyte, echinocyte I, echinocyte II and echinocyte III shapes that are analogous to 3D confocal microscopy imaging observations (refer to section ‘Quantitative validation of CG-RBC membrane model predicted SDE transformation’). A similar approach as in Lim et al. [19, 49] is performed to generate cytoskeletal reference states and the CG-RBC membrane model is adopted to represent only the cytoskeletal spectrin network such that the stable minimum energy state is determined at set reference cytoskeletal surface area ($A_{0, Cyto}$), cytoskeletal volume ($V_{0, Cyto}$) and cytoskeletal reduced volume (v_{Cyto}). $A_{0, Cyto}$ is assumed to be equivalent to that of the RBC (A_0) whereas the reference triangular element surface area of the cytoskeleton, ($A_{k,0, Cyto}$) is set at the corresponding triangular element area at the initial spherical geometry having the radius R_{RBC} . Several $V_{0, Cyto}$ conditions are studied such that $v_{Cyto} = 1.00, 0.99, 0.94, 0.89, 0.83, 0.78, 0.73, 0.68$ and 0.63 . The presence of $E_{Bending}$, in the form of a stronger bending modulus weakens the contribution from shear modulus and leads to an unstressed cytoskeletal state. In addition, the presence of cytoskeletal shear modulus though in weaker form avoids any numerical inconsistency. Therefore, a significantly higher bending modulus ($\kappa = 5.0 \times 10^{-18}$ Nm) is used at the physiological cytoskeletal shear modulus ($\mu_0 = 4.0 \mu\text{Nm}^{-1}$) in order to predict the resultant cytoskeletal equilibrium state. The constraint coefficients; k_A , k_a and k_V are set to $1 \times 10^{-3} \text{Nm}^{-1}$, $5 \times 10^{-5} \text{Nm}^{-1}$ and 100Nm^{-2} , respectively. The influence of any bilayer-leaflet-area-difference and total-membrane-curvature is neglected for cytoskeletal reference state generation. The stress-free equilibrium cytoskeletal state is acknowledged at the minimum free energy state, and corresponding l_0 is extracted at set v_{Cyto} . Next, discocyte, echinocyte I, echinocyte II and echinocyte III predictions described in the section; ‘Quantitative validation of CG-RBC membrane model predicted SDE transformation’, are repeated at estimated l_0 values.

The error (ϵ) is once again estimated for the cellular measurements of H_x , H_z and SF between corresponding experimentally observed and CG-RBC predicted discocyte, echinocyte I, echinocyte II and echinocyte III shapes at stated cytoskeletal reference states. It can be observed (refer to Fig 9) that ϵ is very low for all H_x , H_z and SF cellular measurements at $v_{Cyto} = 0.83, 0.89$ and 0.94 cytoskeletal reference states, whereas ϵ for H_x and H_z is significantly higher at $v_{Cyto} = 1.00$ and 0.99 cytoskeletal reference state conditions. The near spherical cytoskeletal reference state at $v_{Cyto} = 1.00$ and 0.99 results in higher cell thickness, which leads to the significantly higher ϵ at these cytoskeletal reference states.

The qualitative comparison (refer to Fig 10) of CG-RBC predicted discocyte, echinocyte I, echinocyte II and echinocyte III shapes at $v_{Cyto} = 0.83, 0.89$ and 0.94 cytoskeletal reference states, indicates that results at $v_{Cyto} = 0.94$ cytoskeletal reference state agree well with the corresponding experimental observations. There is no significant difference between predicted discocyte shape at $v_{Cyto} = 0.83, 0.89$ and 0.94 . Although the echinocyte I shape at $v_{Cyto} = 0.83$ agrees best with the experimental observation, echinocyte II and echinocyte III shapes at $v_{Cyto} = 0.83$ do not agree well with the corresponding experimental observations. There is no significant difference between predicted echinocyte II shape at $v_{Cyto} = 0.89$ and 0.94 , though the echinocyte III shape at $v_{Cyto} = 0.94$ has evenly distributed spicules over the membrane surface which agrees better with the experimental observations. Therefore, the most likely cytoskeletal

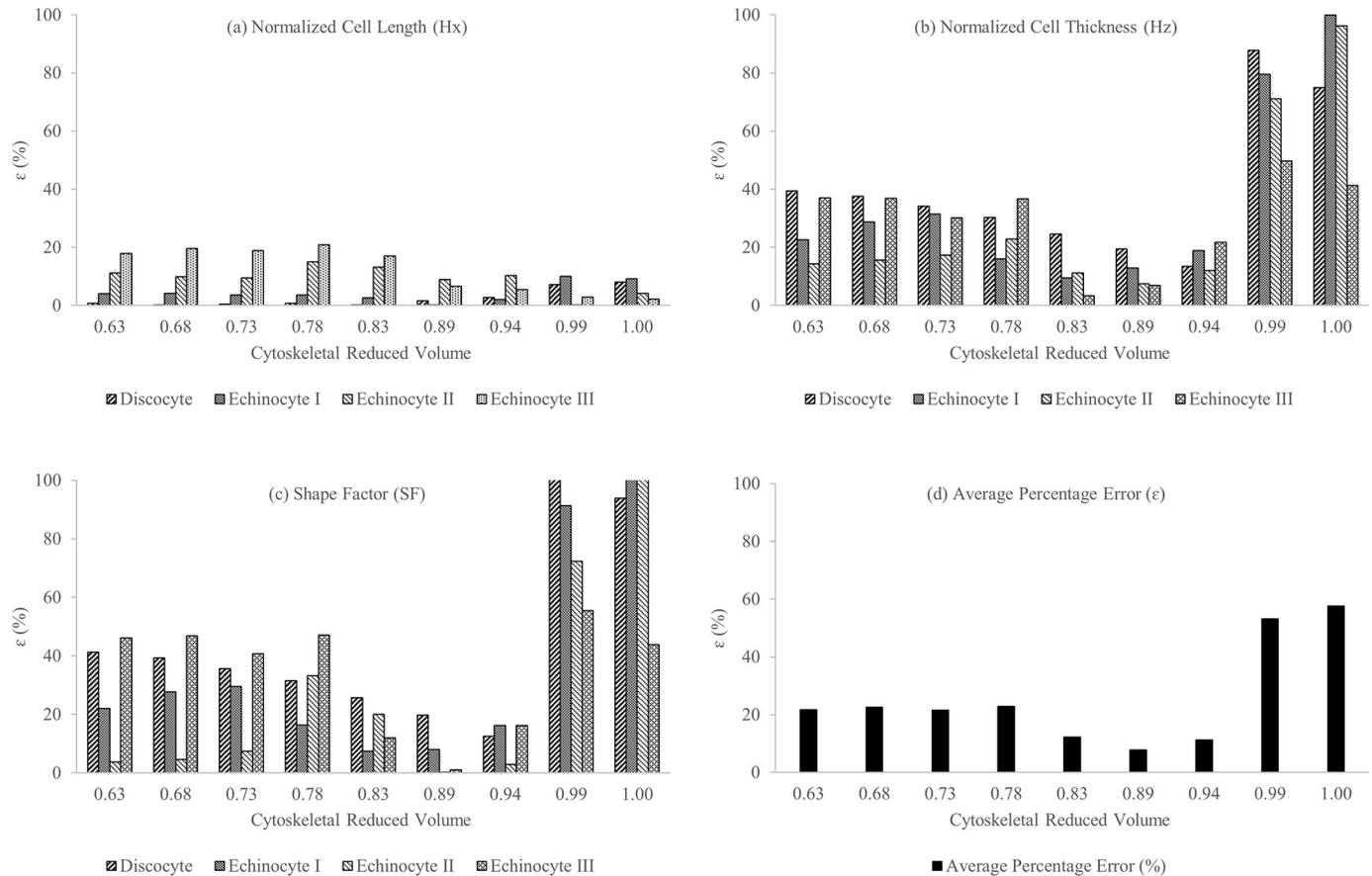


Fig 9. The percentage error (ϵ) for (a) normalized cell length (H_x), (b) normalized cell thickness (H_z), (c) shape factor (SF) and (d) resultant average error between corresponding experimentally observed and CG-RBC predicted discocyte, echinocyte I, echinocyte II and echinocyte III shapes at cytoskeletal reference states of $v_{Cyto} = 1.00, 0.99, 0.94, 0.89, 0.83, 0.78, 0.73, 0.68$ and 0.63 .

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reference state obtained from the CG-RBC membrane model is an ellipsoidal shape at around $v_{Cyto} = 0.94$.

Summary and outlook

A CG-RBC membrane model was developed in this study to improve the understanding of the stomatocyte-discocyte-echinocyte (SDE) transformation of RBC. In contrast to the existing ADE-based numerical simulation methodologies, a bilayer coupling model (BCM)-based membrane bending energy was employed in combination with a new additional constraint: the total-membrane-surface-curvature, in order to predict each stage of stomatocyte IV–echinocyte IV RBC shapes.

The CG-RBC membrane model produced similar RBC shapes with comparison to the existing numerically predicted SDE transformation that were based on either continuum or particle-based approaches. In addition to the commonly used qualitative validation of SDE transformation against experimental observations, a quantitative analysis is conducted in details to evaluate the accuracy and reliability of the shape predictions by the CG-RBC membrane model. Both qualitative and quantitative analyses of the CG-RBC membrane model predicted shapes against the experimentally observed shapes have proved that the newly developed CG-RBC membrane model can predict equivalent RBC shapes with reasonable

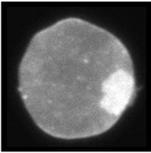
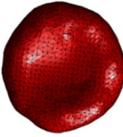
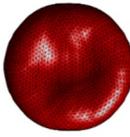
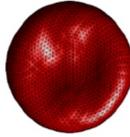
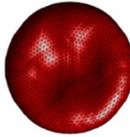
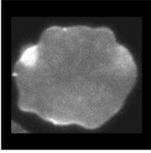
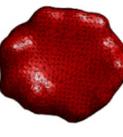
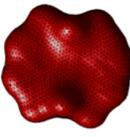
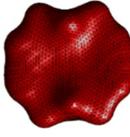
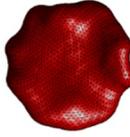
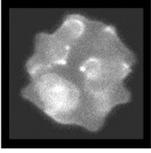
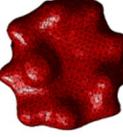
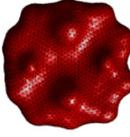
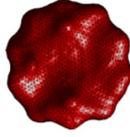
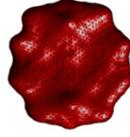
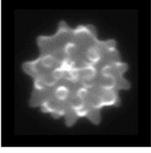
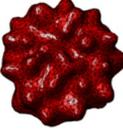
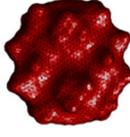
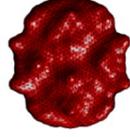
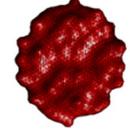
Shape Classification	Experimental Observations (Confocal Microscopy Imaging)	Experimental Observations (Triangulated Surface Mesh)	Numerical Prediction (CG-RBC)			
			$v_{\text{Cyto}} = 0.94$	$v_{\text{Cyto}} = 0.89$	$v_{\text{Cyto}} = 0.83$	
Discocyte						
Echinocyte	I					
	II					
	III					

Fig 10. Qualitative comparison between corresponding experimentally observed and CG-RBC membrane model predicted discocyte, echinocyte I, echinocyte II and echinocyte III shapes at cytoskeletal reference states of $v_{\text{Cyto}} = 1.00, 0.99, 0.94, 0.89, 0.83, 0.78, 0.73, 0.68$ and 0.63 .

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accuracy. The membrane model was then employed to investigate the effect of cell reduced volume (v) and elastic length scale (Λ_{el}). Furthermore, the CG-RBC membrane model was successfully employed to identify the suitability of shape factor (SF) to estimate the deformability of each stage of SDE transformation. The predicted RBC shapes confirmed that the cytoskeletal reference state of the RBC is most likely an ellipsoidal shape, and is agreeable with the numerical predictions by Lim et al. [19, 28, 49] and Khairy and Howard [31] as well.

The CG-RBC membrane model is a general framework to predict the SDE transformation of RBC, and employs a coarse-grained approach to reduce the excessive computational cost for detailed description of the membrane structure. However, the model can be easily refined to represent the detailed RBC membrane structure and any molecular level changes in the presence of shape-transforming agents. The CG-RBC membrane model can be extended to predict the membrane budding and their detachment from RBC to form spherocyte; the RBC shape at higher concentrations of shape-transforming agents or at latter stages of in-vitro RBC storage. Similarly, it is possible to extend the current model to predict the RBC behaviour at defective cytoskeletal conditions; i.e. HE conditions. The equilibrium length of the spectrin links can be set individually, whereas the disruption of vertical connections between lipid-bilayer and cytoskeletal actin junctions can be incorporated into the model by cancelling $E_{\text{Stretching}}$ for the spectrin links attached to these actin junctions. The loss of membrane surface under HS conditions is possible to be introduced to the model by appropriate adjustments to v . However, the cytoskeletal is under compression as it is attached to a lipid-bilayer having a

lower surface area than a healthy cell. Therefore, the cytoskeletal reference state would need adjustments to discuss HS cell behaviour through current CG-RBC membrane model.

In addition, extending the present CG-RBC membrane model to discuss distinct RBC shape-transforming conditions, is a potentially interesting future research avenue. Each shape-transforming agent affects the bilayer-leaflets-area-difference in a unique manner and lead to different stages of SDE transformation. However, the process of changing the area-difference between bilayer-leaflets is unique for each shape-transforming agent. The present CG-RBC membrane model can be extended to incorporate equivalent model parameters at distinct shape-transforming conditions; disease conditions such as HS and HE; occurrence of echinocytic and stomatocytic shape-transforming agents; and RBC aging during in-vitro storage. Furthermore, the proposed CG-RBC membrane model can be easily adapted to consider other hypotheses such as Band 3 conformation [17] and cytoskeleton-bilayer interactions [9] induced RBC shape transformations.

The introduced quantitative analysis framework between experimentally observed and CG-RBC membrane model predicted RBC shapes, forms a feasible approach to better incorporate the biochemical effects into the model. Therefore, the presented CG-RBC membrane model facilitates better understanding of RBC behaviour at different shape-transforming conditions.

Supporting information

S1 Appendix. Methodology for scanning electron microscopy (SEM) imaging for RBC morphology investigations.

(PDF)

S2 Appendix. Methodology for 3D confocal microscopy imaging for RBC morphology investigations.

(PDF)

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Validation: Nadeeshani Maheshika Geekiyanage.

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Writing – original draft: Nadeeshani Maheshika Geekiyanage, Marie Anne Balanant.

Writing – review & editing: Nadeeshani Maheshika Geekiyanage, Marie Anne Balanant, Emilie Sauret, Suvash Saha, Robert Flower, Chwee Teck Lim, YuanTong Gu.

References

1. Buys A.V., et al., Changes in red blood cell membrane structure in type 2 diabetes: a scanning electron and atomic force microscopy study. *Cardiovascular Diabetology*, 2013. 12.
2. Mohandas N. and Gallagher P.G., Red cell membrane: past, present, and future. *Blood*, 2008. 112(10): p. 3939–3948. <https://doi.org/10.1182/blood-2008-07-161166> PMID: 18988878
3. Pretorius E., The adaptability of red blood cells. *Cardiovascular Diabetology*, 2013. 12: p. 63. <https://doi.org/10.1186/1475-2840-12-63> PMID: 23578325
4. Peng Z., Asaro R.J., and Zhu Q., Multiscale simulation of erythrocyte membranes. *Physical Review E*, 2010. 81(3): p. 031904.
5. Tomaiuolo G., Biomechanical properties of red blood cells in health and disease towards microfluidics. *Biomicrofluidics*, 2014. 8(5): p. 051501. <https://doi.org/10.1063/1.4895755> PMID: 25332724
6. Jaferzadeh K. and Moon I., Quantitative investigation of red blood cell three-dimensional geometric and chemical changes in the storage lesion using digital holographic microscopy. *Journal of Biomedical Optics*, 2015. 20(11).
7. Pivkin I.V. and Karniadakis G.E., Accurate coarse-grained modeling of red blood cells. *Physical Review Letters*, 2008. 101(11).
8. Li H. and Lykotrafitis G., Erythrocyte Membrane Model with Explicit Description of the Lipid Bilayer and the Spectrin Network. *Biophysical Journal*, 2014. 107(3): p. 642–653. <https://doi.org/10.1016/j.bpj.2014.06.031> PMID: 25099803
9. Li X., et al., Computational Biomechanics of Human Red Blood Cells in Hematological Disorders. *Journal of Biomechanical Engineering*, 2017. 139(2): p. 021008-1-021008-13.
10. Ademiloye A.S., Zhang L.W., and Liew K.M., Atomistic–continuum model for probing the biomechanical properties of human erythrocyte membrane under extreme conditions. *Computer Methods in Applied Mechanics and Engineering*, 2017. 325: p. 22–36.
11. Igljč A., Kralj-Igljč V., and Hägerstrand H., Amphiphile induced echinocyte-spherocyte transformation of red blood cell shape. *European Biophysics Journal*, 1998. 27(4): p. 335–339. PMID: 9691462
12. Rudenko S.V., Erythrocyte morphological states, phases, transitions and trajectories. *Biochimica et Biophysica Acta—Biomembranes*, 2010. 1798(9): p. 1767–1778.
13. Mukhopadhyay R., Lim G., and Wortis M., Echinocyte shapes: Bending, stretching, and shear determine spicule shape and spacing. *Biophysical Journal*, 2002. 82(4): p. 1756–1772. PMID: 11916836
14. Rudenko S.V. and Saeid M.K., Reconstruction of erythrocyte shape during modified morphological response. *Biochemistry (Moscow)*, 2010. 75(8): p. 1025–1031.
15. Chen M. and Boyle F.J., An Enhanced Spring-Particle Model for Red Blood Cell Structural Mechanics: Application to the Stomatocyte–Discocyte–Echinocyte Transformation. *Journal of Biomechanical Engineering*, 2017. 139(12): p. 121009-1-121009-11.
16. Etcheverry S., et al., Real-time study of shape and thermal fluctuations in the echinocyte transformation of human erythrocytes using defocusing microscopy. *Journal of Biomedical Optics*, 2012. 17(10).
17. Wong P., A basis of echinocytosis and stomatocytosis in the disc–sphere transformations of the erythrocyte. *Journal of Theoretical Biology*, 1999. 196(3): p. 343–361. <https://doi.org/10.1006/jtbi.1998.0845> PMID: 10049626
18. Gedde M.M. and Huestis W.H., Membrane potential and human erythrocyte shape. *Biophysical Journal*, 1997. 72(3): p. 1220–1233. [https://doi.org/10.1016/S0006-3495\(97\)78769-1](https://doi.org/10.1016/S0006-3495(97)78769-1) PMID: 9138568
19. Lim H. Wortis W. G., M., and Mukhopadhyay R., Red Blood Cell Shapes and Shape Transformations: Newtonian Mechanics of a Composite Membrane: Sections 2.5–2.8, in *Soft Matter*. 2009, Wiley-VCH Verlag GmbH & Co. KGaA. p. 83–250. <https://doi.org/10.1140/epje/i2009-10510-y>

20. Tachev K.D., Danov K.D., and Kralchevsky P.A., On the mechanism of stomatocyte-echinocyte transformations of red blood cells: Experiment and theoretical model. *Colloids and Surfaces B: Biointerfaces*, 2004. 34(2): p. 123–140. <https://doi.org/10.1016/j.colsurfb.2003.12.011> PMID: 15261082
21. Sheetz M.P. and Singer S.J., Biological membranes as bilayer couples: Molecular mechanisms of drug-erythrocyte interactions. *Proceedings of the National Academy of Sciences of the United States of America*, 1974. 71(11): p. 4457–4461. PMID: 4530994
22. Gedde M.M., Yang E., and Huestis W.H., Resolution of the paradox of red cell shape changes in low and high pH. *Biochimica et Biophysica Acta (BBA)—Biomembranes*, 1999. 1417(2): p. 246–253.
23. Miao L., et al., Budding transitions of fluid-bilayer vesicles: The effect of area-difference elasticity. *Physical Review E*, 1994. 49(6): p. 5389–5407.
24. Seifert Udo, Berndt Karin, and R. Lipowsky, Shape transformations of vesicles: Phase diagram for spontaneous-curvature and bilayer-coupling models. *Physical Review A*, 1991. 44(2): p. 1182–1202.
25. Brecher G. and Bessis M., Present Status of Spiculed Red Cells and Their Relationship to the Discocyte-Echinocyte Transformation: A Critical Review. *Blood*, 1972. 40(3): p. 333. PMID: 5056966
26. Bessis M. Red Cell Shapes. An Illustrated Classification and its Rationale. in *Red Cell Shape*. 1973. Berlin, Heidelberg: Springer Berlin Heidelberg.
27. Svetina S. and Žekš B., Membrane bending energy and shape determination of phospholipid vesicles and red blood cells. *European Biophysics Journal*, 1989. 17(2): p. 101–111. PMID: 2766997
28. Lim H. Wortis W. G., M., and Mukhopadhyay R., Stomatocyte–discocyte–echinocyte sequence of the human red blood cell: Evidence for the bilayer–couple hypothesis from membrane mechanics. *Proceedings of the National Academy of Sciences of the United States of America*, 2002. 99(26): p. 16766–16769. <https://doi.org/10.1073/pnas.202617299> PMID: 12471152
29. Kuzman D., et al., Elastic properties of the red blood cell membrane that determine echinocyte deformability. *European Biophysics Journal*, 2004. 33(1): p. 1–15. <https://doi.org/10.1007/s00249-003-0337-4> PMID: 13680208
30. Svetina S., et al., The cooperative role of membrane skeleton and bilayer in the mechanical behaviour of red blood cells. *Bioelectrochemistry*, 2004. 62(2): p. 107–113. <https://doi.org/10.1016/j.bioelechem.2003.08.002> PMID: 15039011
31. Khairy K., Foo J., and Howard J., Shapes of Red Blood Cells: Comparison of 3D Confocal Images with the Bilayer-Couple Model. *Cellular and Molecular Bioengineering*, 2008. 1(2): p. 173.
32. Pages G., Yau T.W., and Kuchel P.W., Erythrocyte shape reversion from echinocytes to discocytes: Kinetics via fast-measurement NMR diffusion-diffraction. *Magnetic Resonance in Medicine*, 2010. 64(3): p. 645–652. <https://doi.org/10.1002/mrm.22457> PMID: 20806372
33. Khairy K. and Howard J., Minimum-energy vesicle and cell shapes calculated using spherical harmonics parameterization. *Soft Matter*, 2011. 7(5): p. 2138–2143.
34. Tong Z.-X., et al., Coarse-grained area-difference-elasticity membrane model coupled with IB–LB method for simulation of red blood cell morphology. *Physica A: Statistical Mechanics and its Applications*, 2018. 509: p. 1183–1194.
35. Ju M., et al., A review of numerical methods for red blood cell flow simulation. *Computer Methods in Biomechanics and Biomedical Engineering*, 2015. 18(2): p. 130–140. <https://doi.org/10.1080/10255842.2013.783574> PMID: 23582050
36. Ye T., Phan-Thien N., and Lim C.T., Particle-based simulations of red blood cells—A review. *Journal of Biomechanics*, 2016. 49(11): p. 2255–2266. <https://doi.org/10.1016/j.jbiomech.2015.11.050> PMID: 26706718
37. Polwaththe-Gallage H.N., et al., A coupled SPH-DEM approach to model the interactions between multiple red blood cells in motion in capillaries. *International Journal of Mechanics and Materials in Design*, 2015: p. 1–18.
38. Barns S., et al., Investigation of red blood cell mechanical properties using AFM indentation and coarse-grained particle method. *Biomed Eng Online*, 2017. 16(1): p. 140. <https://doi.org/10.1186/s12938-017-0429-5> PMID: 29258590
39. Zhang L., Feng X., and Li S., Review and perspective on soft matter modeling in cellular mechanobiology: cell contact, adhesion, mechanosensing, and motility. *Acta Mechanica*, 2017. 228(12): p. 4095–4122.
40. Gong X., et al., The deformation behavior of multiple red blood cells in a capillary vessel. *Journal of Biomechanical Engineering*, 2009. 131(7): p. 074504. <https://doi.org/10.1115/1.3127255> PMID: 19640140
41. Marcelli G., Parker K.H., and Winlove C.P., Thermal fluctuations of red blood cell membrane via a constant-area particle-dynamics model. *Biophysical Journal*, 2005. 89(4): p. 2473–2480. <https://doi.org/10.1529/biophysj.104.056168> PMID: 16055528

42. Li X., Vlahovska P.M., and Karniadakis G.E., Continuum- and particle-based modeling of shapes and dynamics of red blood cells in health and disease. *Soft Matter*, 2013. 9(1): p. 28–37. <https://doi.org/10.1039/C2SM26891D> PMID: 23230450
43. Helfrich W., Blocked lipid exchange in bilayers and its possible influence on the shape of vesicles. *Z Naturforsch C*, 1974. 29c(9–10): p. 510–5.
44. Helfrich W., Elastic properties of lipid bilayers: theory and possible experiments. *Zeitschrift fur Naturforschung. Teil C: Biochemie, Biophysik, Biologie, Virologie*, 1973. 28(11): p. 693–703.
45. Svetina S., Ottova-Leitmannova A., and Glaser R., Membrane bending energy in relation to bilayer couples concept of red blood cell shape transformations. *Journal of Theoretical Biology*, 1982. 94(1): p. 13–23. PMID: 7078204
46. Heinrich V., Svetina S., and Žekš B., Nonaxisymmetric vesicle shapes in a generalized bilayer-couple model and the transition between oblate and prolate axisymmetric shapes. *Physical Review E*, 1993. 48(4): p. 3112–3123.
47. Li X., et al., Shape Transformations of Membrane Vesicles from Amphiphilic Triblock Copolymers: A Dissipative Particle Dynamics Simulation Study. *Macromolecules*, 2009. 42(8): p. 3195–3200.
48. Svetina S., Vesicle budding and the origin of cellular life. *Chemphyschem*, 2009. 10(16): p. 2769–76. <https://doi.org/10.1002/cphc.200900577> PMID: 19774545
49. Lim G.H.W., A Numerical Study of Morphologies and Morphological Transformations of Human Erythrocyte Based on Membrane Mechanics, in Department of Physics. 2003, Simon Fraser University.
50. Fedosov D.A., Caswell B., and Karniadakis G.E., Systematic coarse-graining of spectrin-level red blood cell models. *Computer Methods in Applied Mechanics and Engineering*, 2010. 199(29–32): p. 1937–1948.
51. Li H. and Lykotrafitis G., Vesiculation of healthy and defective red blood cells. *Physical Review E*, 2015. 92(1): p. 012715.
52. Li H., et al., Mechanics of diseased red blood cells in human spleen and consequences for hereditary blood disorders. *Proceedings of the National Academy of Sciences*, 2018. 115(38): p. 9574.
53. Nakamura M., Bessho S., and Wada S., Analysis of red blood cell deformation under fast shear flow for better estimation of hemolysis. *International Journal for Numerical Methods in Biomedical Engineering*, 2014. 30(1): p. 42–54. <https://doi.org/10.1002/cnm.2587> PMID: 23949912
54. Tsubota K.-i., Short note on the bending models for a membrane in capsule mechanics: Comparison between continuum and discrete models. *Journal of Computational Physics*, 2014. 277: p. 320–328.
55. Tsubota K.-i. and Wada S., Elastic force of red blood cell membrane during tank-treading motion: Consideration of the membrane's natural state. *International Journal of Mechanical Sciences*, 2010. 52(2): p. 356–364.
56. Hashemi Z. and Rahnema M., Dynamic Response of a Red Blood Cell in Shear Flow. *AUT Journal of Mechanical Engineering*, 2017. 1(2): p. 233–242.
57. Fedosov, D.A., et al., Coarse-Grained Red Blood Cell Model with Accurate Mechanical Properties, Rheology and Dynamics, in Annual International Conference of the IEEE Engineering in Medicine and Biology Society. 2009. p. 4266–4269.
58. Rodriguez J., Edeskär T., and Knutsson S., Particle shape quantities and measurement techniques: a review. *The Electronic journal of geotechnical engineering*, 2013. 18/A: p. 169–198.
59. Monzel C. and Sengupta K., Measuring shape fluctuations in biological membranes. *Journal of Physics D-Applied Physics*, 2016. 49(24): p. 21.
60. Li J., et al., Spectrin-Level Modeling of the Cytoskeleton and Optical Tweezers Stretching of the Erythrocyte. *Biophysical Journal*, 2005. 88(5): p. 3707–3719. <https://doi.org/10.1529/biophysj.104.047332> PMID: 15749778
61. Song H., et al., Study of in vitro RBCs membrane elasticity with AOD scanning optical tweezers. *Biomedical Optics Express*, 2017. 8(1): p. 384–394. <https://doi.org/10.1364/BOE.8.000384> PMID: 28101425
62. Yoon D. and You D., Continuum modeling of deformation and aggregation of red blood cells. *Journal of Biomechanics*, 2016. 49(11): p. 2267–2279. <https://doi.org/10.1016/j.jbiomech.2015.11.027> PMID: 26706720
63. Chang H.-Y., et al., MD/DPD Multiscale Framework for Predicting Morphology and Stresses of Red Blood Cells in Health and Disease. *PLOS Computational Biology*, 2016. 12(10): p. e1005173. <https://doi.org/10.1371/journal.pcbi.1005173> PMID: 27792725
64. Frank S.M., et al., Decreased erythrocyte deformability after transfusion and the effects of erythrocyte storage duration. *Anesthesia and Analgesia*, 2013. 116(5): p. 975–981. <https://doi.org/10.1213/ANE.0b013e31828843e6> PMID: 23449853