

# Hydromagnetic Steady Flow of Maxwell Fluid over a Bidirectional Stretching Surface with Prescribed Surface Temperature and Prescribed Surface Heat Flux

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## Abstract

This paper investigates the steady hydromagnetic three-dimensional boundary layer flow of Maxwell fluid over a bidirectional stretching surface. Both cases of prescribed surface temperature (PST) and prescribed surface heat flux (PHF) are considered. Computations are made for the velocities and temperatures. Results are plotted and analyzed for PST and PHF cases. Convergence analysis is presented for the velocities and temperatures. Comparison of PST and PHF cases is given and examined.

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## Introduction

Interest of recent researchers in analysis of boundary layer flows over a continuously moving surface with prescribed surface temperature or heat flux has increased substantially during the last few decades. These flows have abundant applications in many metallurgical and industrial processes. Specific examples of such industrial and technological processes include wire-drawing, glass-fiber and paper production, the extrusion of polymer sheets, the cooling of a metallic plate in a cooling bath, drawing of plastic films etc. Such situations occur in the class of flow problems relevant to the polymer extrusion in which the flow is generated by stretching of plastic surface [1,2]. In addition, internal heat generation/absorption has key role in the heat transfer from a heated sheet in several practical aspects. The heat generation/absorption effects are also important in the flow problems dealing with the dissociating fluids. Influences of heat generation/absorption may change the temperature distribution which corresponds to the particle deposition rate in electronic chips, nuclear reactors, semiconductor wafers etc. The idea of boundary layer flow over a moving surface was introduced by Sakiadis [3]. He discussed the boundary layer flow of viscous fluid over a solid surface. This analysis was extended by Crane [4] for a linearly stretched surface. He provided the closed form solutions of two-dimensional boundary layer flow of viscous fluid over a surface. Numerous literature now exists on the boundary layer flow with heat transfer and in the presence of heat generation/absorption effects (see [5–10] and many refs. therein).

A large number of industrial fluids like polymers, soaps, molten plastics, sugar solutions pulps, apple sauce, drilling muds etc. behave as the non-Newtonian fluids [11]. The Navier-Stokes

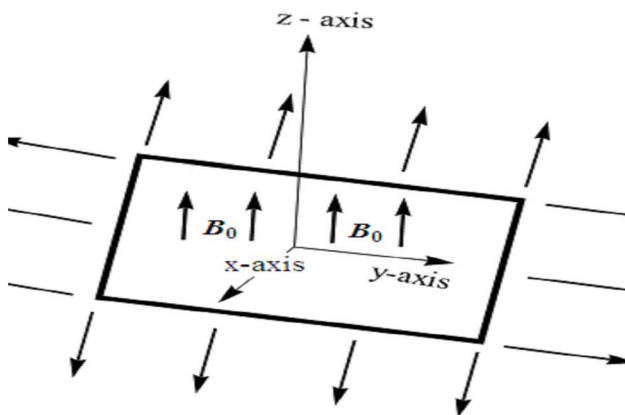
equations cannot explore the properties of such materials. In the literature, different types of fluids models are developed according to the nature of fluids. The non-Newtonian fluids are mainly divided into three categories which are known as the differential, rate and integral types. The fluid considered here is called the Maxwell fluid. It is subclass of rate type fluids predicting the characteristics of relaxation time. The properties of polymeric fluids can be explored by Maxwell model for small relaxation time. Zierep and Fetecau [12] discussed the energetic balance for the Rayleigh-Stokes problem involving Maxwell fluid. Closed form solutions of unsteady flow of Maxwell fluid due to the sudden movement of the plate was described by Hayat et al. [13]. Fetecau et al. [14] provided the exact solutions for the unsteady flow of Maxwell fluid. Here they considered that the flow is generated due to the constantly accelerating plate. Flow of Maxwell fluid with fractional derivative model between two coaxial cylinders was also addressed by Fetecau et al. [15]. Here the inner cylinder is subjected to the time-dependent longitudinal shear stress generating the fluid motion. Helical unidirectional flows of Maxwell fluid due to shear stresses on the boundary have been studied by Jamil and Fetecau [16]. They provided the exact solution by Hankel transform method. Stability analysis for the flow of Maxwell fluid under solet-driven double-diffusive convection in a porous medium was examined by Wang and Tan [17]. Two-dimensional boundary layer flow of Maxwell fluid over a linearly stretching surface was analyzed by Hayat et al. [18]. Mukhopadhyay [19] presented an analysis for the unsteady flow of Maxwell fluid in a porous medium with suction/injection. Falkner-Skan flow of Maxwell fluid with mixed convection over a surface was analytically discussed by Hayat et al. [20].

The main theme of present analysis is to discuss the steady three-dimensional boundary layer flow of Maxwell fluid over a bidirectional stretching surface subject to prescribed surface temperature and prescribed surface heat flux. The effects of applied magnetic field are also included in this analysis. To our knowledge, not much is known about flows induced by a bidirectional stretching surface. Wang [21] discussed the three-dimensional flow of viscous fluid over a bidirectional stretching surface. Ariel [22] provided the exact and homotopy perturbation solution for ref. [21]. Liu and Andersson [23] discussed the heat transfer analysis over a bidirectional stretching surface with variable thermal conditions. Ahmed et al. [24] extended the analysis of ref. [23] for hydromagnetic flow in a porous medium. They presented the series solutions. Hayat et al. and Shehzad et al. [25,26] studied the boundary layer flows of Maxwell and Jeffery fluids over a bidirectional stretching surface. The present analysis is arranged as follows. The next section contains the mathematical formulation of the problem. Sections three and four are for the homotopy solutions (HAM) [27–34], convergence study and discussion. Both cases of prescribed surface temperature (PST) and prescribed surface heat flux (PHF) are given due attention in the discussion section. The main observations of this research are listed in the last section. Further, the correct modelling for magnetohydrodynamic case of Maxwell fluid is given.

**Flow Model**

Consider three-dimensional magnetohydrodynamic (MHD) boundary layer flow of an incompressible Maxwell fluid. The flow is induced by bidirectional stretching surface (at  $z=0$ ) with PST and PHF. Steady flow of an incompressible Maxwell fluid is considered for  $z>0$ . Flow analysis is carried out in the presence of heat generation/absorption parameter. The fluid is electrically conducting in the presence of applied magnetic field with constant strength  $B_0$ . No electric field contribution is taken into account. Induced magnetic field effects are ignored through large magnetic Reynolds number consideration. The geometry of considered flow is shown in Fig. 1. The conservation of mass, momentum and energy for steady flow in presence of magnetic field and heat source/sink can be expressed as

$$\text{div}\mathbf{V}=0, \tag{1}$$



**Figure 1. Physical model.**  
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$$\rho \frac{d\mathbf{V}}{dt} = \text{div}\mathbf{T} + \mathbf{J} \times \mathbf{B}, \tag{2}$$

$$\rho c_p \frac{dT}{dt} = \mathbf{T} \cdot \nabla \mathbf{V} + k \nabla^2 T + Q(T - T_\infty), \tag{3}$$

in which  $\rho$  depicts the density,  $\mathbf{J}$  the current density,  $\mathbf{B}$  the magnetic field in the  $z$ - direction,  $c_p$  the specific heat,  $k$  the thermal conductivity and  $Q$  the heat generation/absorption parameter with  $Q>0$  (heat generation) and  $Q<0$  (heat absorption).  $\mathbf{B} = B_0 \hat{k}$  ( $\hat{k}$  is a unit vector parallel to the  $z$ - axis). The definition of  $\mathbf{J}$  for present flow consideration is

$$\mathbf{J} = \sigma(\mathbf{V} \times \mathbf{B}_0), \tag{4}$$

where  $\mathbf{V}$  denotes the fluid velocity and  $\sigma$  the electrical conductivity. The Lorentz force thus reduces to

$$\mathbf{J} \times \mathbf{B} = -\sigma B_0^2 \mathbf{V}. \tag{5}$$

Expressions of Cauchy ( $\mathbf{T}$ ) and extra stress ( $\mathbf{S}$ ) tensors in Maxwell fluid are [11]:

$$\mathbf{T} = -p\mathbf{I} + \mathbf{S}, \tag{6}$$

$$\mathbf{S} + \lambda_1 \frac{D\mathbf{S}}{Dt} = \mu \mathbf{A}_1, \tag{7}$$

where  $D/Dt$  is the Covariant differentiation and  $\lambda_1$  is the relaxation time. The first Rivlin Ericksen tensor  $\mathbf{A}_1$  is defined as

$$\mathbf{A}_1 = \text{grad}\mathbf{V} + (\text{grad}\mathbf{V})^*,$$

where  $*$  indicates the matrix transpose and the velocity field  $\mathbf{V}$  here is taken as

$$\mathbf{V} = [u(x, y, z), v(x, y, z), w(x, y, z)]. \tag{8}$$

The definition of  $D/Dt$  is [11]

$$\frac{Da_i}{Dt} = \frac{\partial a_i}{\partial t} + u_r a_{i,r} - u_{i,r} a_r. \tag{9}$$

Following the procedure of ref. [11] at pages 221–223 and using above equations, we have the following scalar expressions

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{10}$$

$$\begin{aligned}
 & u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \lambda_1 \left( u^2 \frac{\partial^2 u}{\partial x^2} + v^2 \frac{\partial^2 u}{\partial y^2} + w^2 \frac{\partial^2 u}{\partial z^2} + 2uv \frac{\partial^2 u}{\partial x \partial y} \right. \\
 & \quad \left. + 2vw \frac{\partial^2 u}{\partial y \partial z} + 2uw \frac{\partial^2 u}{\partial x \partial z} \right) = \\
 & - \frac{\partial p}{\partial x} + v \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) - \frac{\sigma B_0^2}{\rho} u - \\
 & \frac{\sigma B_0^2}{\rho} \lambda_1 \left( u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} - u \frac{\partial u}{\partial x} \right),
 \end{aligned} \tag{11}$$

$$\begin{aligned}
 & u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \lambda_1 \left( u^2 \frac{\partial^2 v}{\partial x^2} + v^2 \frac{\partial^2 v}{\partial y^2} + w^2 \frac{\partial^2 v}{\partial z^2} + 2uv \frac{\partial^2 v}{\partial x \partial y} \right) \\
 & \quad \left. + 2vw \frac{\partial^2 v}{\partial y \partial z} + 2uw \frac{\partial^2 v}{\partial x \partial z} \right) \\
 & = - \frac{\partial p}{\partial y} + v \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) - \frac{\sigma B_0^2}{\rho} v \\
 & - \frac{\sigma B_0^2}{\rho} \lambda_1 \left( u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} - v \frac{\partial v}{\partial y} \right),
 \end{aligned} \tag{12}$$

$$\begin{aligned}
 & u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} + \lambda_1 \left( u^2 \frac{\partial^2 w}{\partial x^2} + v^2 \frac{\partial^2 w}{\partial y^2} + w^2 \frac{\partial^2 w}{\partial z^2} + 2uv \frac{\partial^2 w}{\partial x \partial y} \right) \\
 & \quad \left. + 2vw \frac{\partial^2 w}{\partial y \partial z} + 2uw \frac{\partial^2 w}{\partial x \partial z} \right) \\
 & = - \frac{\partial p}{\partial z} + v \left( \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right),
 \end{aligned} \tag{13}$$

$$\begin{aligned}
 u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} &= k_1 \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) \\
 &+ \frac{Q}{\rho c_p} (T - T_\infty).
 \end{aligned} \tag{14}$$

After employing the boundary layer assumptions [35], the above equations in the absence of pressure gradient yield

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{15}$$

$$\begin{aligned}
 & u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = v \left( \frac{\partial^2 u}{\partial z^2} \right) - \\
 & \lambda_1 \left( u^2 \frac{\partial^2 u}{\partial x^2} + v^2 \frac{\partial^2 u}{\partial y^2} + w^2 \frac{\partial^2 u}{\partial z^2} + 2uv \frac{\partial^2 u}{\partial x \partial y} \right. \\
 & \quad \left. + 2vw \frac{\partial^2 u}{\partial y \partial z} + 2uw \frac{\partial^2 u}{\partial x \partial z} \right) - \frac{\sigma B_0^2}{\rho} \left( u + \lambda_1 w \frac{\partial u}{\partial z} \right),
 \end{aligned} \tag{16}$$

$$\begin{aligned}
 & u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = v \left( \frac{\partial^2 v}{\partial z^2} \right) - \\
 & \lambda_1 \left( u^2 \frac{\partial^2 v}{\partial x^2} + v^2 \frac{\partial^2 v}{\partial y^2} + w^2 \frac{\partial^2 v}{\partial z^2} + 2uv \frac{\partial^2 v}{\partial x \partial y} + \right. \\
 & \quad \left. 2vw \frac{\partial^2 v}{\partial y \partial z} + 2uw \frac{\partial^2 v}{\partial x \partial z} \right) - \frac{\sigma B_0^2}{\rho} \left( v + \lambda_1 w \frac{\partial v}{\partial z} \right),
 \end{aligned} \tag{17}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = k_1 \frac{\partial^2 T}{\partial z^2} + \frac{Q}{\rho c_p} (T - T_\infty). \tag{18}$$

The associated boundary conditions are defined as follows.

$$\begin{aligned}
 & u = u_w(x) = ax, v = v_w(y) = by, w = 0 \text{ at } z = 0, \\
 & u \rightarrow 0, v \rightarrow 0 \text{ as } z \rightarrow \infty.
 \end{aligned} \tag{19}$$

For temperature, the boundary conditions are specified as [23,24]:

**Type i.** Prescribed surface temperature (PST)

$$\begin{aligned}
 & T = T_w(x, y) = T_\infty + Cx^r y^s \text{ at } z = 0, \\
 & T \rightarrow T_\infty \text{ as } y \rightarrow \infty.
 \end{aligned} \tag{20}$$

**Type ii.** Prescribed surface heat flux (PHF)

$$\begin{aligned}
 & -k \frac{\partial T}{\partial z} = Dx^r y^s \text{ at } z = 0, \\
 & T \rightarrow T_\infty \text{ as } y \rightarrow \infty.
 \end{aligned} \tag{21}$$

Here  $k$  is the thermal conductivity of the fluid,  $T_\infty$  the constant temperature outside the thermal boundary layer,  $C$  and  $D$  the positive constants. The power indices  $r$  and  $s$  determine how the temperature or the heat flux varies in the  $xy$ - plane.

Following [23,24] similarity variables for the velocity field are introduced as

$$u = axf'(\eta), v = ayg'(\eta), w = -\sqrt{av}(f(\eta) + g(\eta)), \eta = z\sqrt{\frac{a}{\nu}} \tag{22}$$

and the temperature similarity variables take different forms depending on the boundary conditions being considered. These are

$$\begin{aligned}
 & PST : \theta(\eta) = \frac{T(x, y, z) - T_\infty}{T_w(x, y) - T_\infty}, PHF : T(x, y, z) - T_\infty \\
 & = \frac{B}{k} \sqrt{\frac{\nu}{a}} x^r y^s \phi(\eta)
 \end{aligned} \tag{23}$$

equation (15) is automatically satisfied and Eqs. (16)–(21) take the following forms:

$$f''' + (M^2\beta + 1)(f + g)f'' - f'^2 + \beta(2(f + g)f'f'' - (f + g)^2f''') - M^2f' = 0, \tag{24}$$

$$g''' + (M^2\beta + 1)(f + g)g'' - g'^2 + \beta(2(f + g)g'g'' - (f + g)^2g''') - M^2g' = 0, \tag{25}$$

$$\theta'' + \text{Pr}(f + g)\theta' + \text{Pr}(B - rf' - sg')\theta = 0, \tag{26}$$

$$\phi'' + \text{Pr}(f + g)\phi' + \text{Pr}(B - rf' - sg')\phi = 0, \tag{27}$$

$$f = 0, g = 0, f' = 1, g' = \alpha, \theta = 1, \phi' = -1 \text{ at } \eta = 0, \\ f' \rightarrow 0, g' \rightarrow 0, \theta \rightarrow 0, \phi \rightarrow 0 \text{ as } \eta \rightarrow \infty, \tag{28}$$

where  $\beta_1 = \lambda_1 a$  is the Deborah number,  $M = \frac{\sigma B_0^2}{a\rho}$  the magnetic parameter,  $\alpha = \frac{b}{a}$  the ratio of stretching rates,  $\text{Pr} = \frac{\nu}{k_1}$  the Prandtl number,  $k_1$  the thermal diffusivity and  $B = \frac{Q}{\rho a c_p}$  the internal heat parameter.

### Homotopy Analysis Solutions

In this section, we solve the problem consisting of Eqs. (24)–(27) with boundary conditions in Eq. (28) by HAM. For that the initial guesses and auxiliary linear operators are taken as follows:

$$f_0(\eta) = (1 - e^{-\eta}), g_0(\eta) = \alpha(1 - e^{-\eta}), \\ \theta_0(\eta) = \exp(-\eta), \phi_0(\eta) = \exp(-\eta), \tag{29}$$

$$L_f = f''' - f', L_g = g''' - g', L_\theta = \theta'' - \theta, L_\phi = \phi'' - \phi, \tag{30}$$

subject to the properties

$$L_f(C_1 + C_2e^\eta + C_3e^{-\eta}) = 0, L_g(C_4 + C_5e^\eta + C_6e^{-\eta}) = 0, \\ L_\theta(C_7e^\eta + C_8e^{-\eta}) = 0, L_\phi(C_9e^\eta + C_{10}e^{-\eta}) = 0, \tag{31}$$

where  $C_i$  ( $i = 1 - 10$ ) are the arbitrary constants.

At zeroth order, the problems satisfy

$$(1 - p)L_f(\hat{f}(\eta; p) - f_0(\eta)) = p\hbar_f \mathbf{N}_f(\hat{f}(\eta; p), \hat{g}(\eta; p)), \tag{32}$$

$$(1 - p)L_g(\hat{g}(\eta; p) - g_0(\eta)) = p\hbar_g \mathbf{N}_g(\hat{f}(\eta; p), \hat{g}(\eta; p)), \tag{33}$$

$$(1 - p)L_\theta(\hat{\theta}(\eta; p) - \theta_0(\eta)) = p\hbar_\theta \mathbf{N}_\theta(\hat{f}(\eta; p), \hat{g}(\eta; p), \hat{\theta}(\eta; p)), \tag{34}$$

$$(1 - p)L_\phi(\hat{\phi}(\eta; p) - \phi_0(\eta)) = p\hbar_\phi \mathbf{N}_\phi(\hat{f}(\eta; p), \hat{g}(\eta; p), \hat{\phi}(\eta; p)), \tag{35}$$

$$\hat{f}(0; p) = 0, \hat{f}'(0; p) = 1, \hat{f}'(\infty; p) = 0, \hat{g}(0; p) = 0, \hat{g}'(0; p) = \alpha, \\ \hat{g}'(\infty; p) = 0, \hat{\theta}(0; p) = 1, \hat{\theta}(\infty; p) = 0, \hat{\phi}(0; p) = 0, \hat{\phi}(\infty; p) = 0, \tag{36}$$

$$\mathbf{N}_f[\hat{f}(\eta, p), \hat{g}(\eta, p)] = \frac{\partial^3 \hat{f}(\eta, p)}{\partial \eta^3} - \left( \frac{\partial \hat{f}(\eta, p)}{\partial \eta} \right)^2 \\ + (M^2\beta + 1)(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial^2 \hat{f}(\eta, p)}{\partial \eta^2} \\ + \beta \left( \begin{aligned} &2(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial \hat{f}(\eta, p)}{\partial \eta} \frac{\partial^2 \hat{f}(\eta, p)}{\partial \eta^2} \\ & - (\hat{f}(\eta, p) + \hat{g}(\eta, p))^2 \frac{\partial^3 \hat{f}(\eta, p)}{\partial \eta^3} \end{aligned} \right) \\ - M^2 \frac{\partial \hat{f}(\eta, p)}{\partial \eta}, \tag{37}$$

$$\mathbf{N}_g[\hat{g}(\eta, p), \hat{f}(\eta, p)] = \frac{\partial^3 \hat{g}(\eta, p)}{\partial \eta^3} - \left( \frac{\partial \hat{g}(\eta, p)}{\partial \eta} \right)^2 \\ + (M^2\beta + 1)(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial^2 \hat{g}(\eta, p)}{\partial \eta^2} \\ + \beta \left( \begin{aligned} &2(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial \hat{g}(\eta, p)}{\partial \eta} \frac{\partial^2 \hat{g}(\eta, p)}{\partial \eta^2} \\ & - (\hat{f}(\eta, p) + \hat{g}(\eta, p))^2 \frac{\partial^3 \hat{g}(\eta, p)}{\partial \eta^3} \end{aligned} \right) \\ - M^2 \frac{\partial \hat{g}(\eta, p)}{\partial \eta}, \tag{38}$$

$$\mathbf{N}_\theta[\hat{\theta}(\eta, p), \hat{f}(\eta, p), \hat{g}(\eta, p)] = \frac{\partial^2 \hat{\theta}(\eta, p)}{\partial \eta^2} \\ + \text{Pr}(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial \hat{\theta}(\eta, p)}{\partial \eta} \\ + \text{Pr} \left( \beta - \gamma \frac{\partial \hat{f}(\eta, p)}{\partial \eta} - s \frac{\partial \hat{g}(\eta, p)}{\partial \eta} \right) \hat{\theta}(\eta, p), \tag{39}$$

$$\mathbf{N}_\phi[\hat{\phi}(\eta, p), \hat{f}(\eta, p), \hat{g}(\eta, p)] = \frac{\partial^2 \hat{\phi}(\eta, p)}{\partial \eta^2} \\ + \text{Pr}(\hat{f}(\eta, p) + \hat{g}(\eta, p)) \frac{\partial \hat{\phi}(\eta, p)}{\partial \eta} \\ + \text{Pr} \left( \beta - \gamma \frac{\partial \hat{f}(\eta, p)}{\partial \eta} - s \frac{\partial \hat{g}(\eta, p)}{\partial \eta} \right) \hat{\phi}(\eta, p). \tag{40}$$

In above expressions,  $p$  shows the embedding parameter,  $\hat{h}_f, \hat{h}_g, \hat{h}_\theta$  and  $\hat{h}_\phi$  the non-zero auxiliary parameters and  $\mathbf{N}_f, \mathbf{N}_g, \mathbf{N}_\theta$  and  $\mathbf{N}_\phi$  the nonlinear operators. When  $p=0$  and  $p=1$  then we obtain

$$\begin{aligned} \hat{f}(\eta; 0) &= f_0(\eta), \hat{g}(\eta, 0) = g_0(\eta), \hat{\theta}(\eta, 0) = \theta_0(\eta), \hat{\phi}(\eta, 0) = \phi_0(\eta), \\ \hat{f}(\eta; 1) &= f(\eta), \hat{g}(\eta, 1) = g(\eta), \hat{\theta}(\eta, 1) = \theta(\eta), \hat{\phi}(\eta, 1) = \phi(\eta). \end{aligned} \tag{41}$$

It should be pointed out that when  $p$  increases from 0 to 1 then  $f(\eta, p), g(\eta, p), \theta(\eta, p)$  and  $\phi(\eta, p)$  vary from  $f_0(\eta), g_0(\eta), \theta_0(\eta), \phi_0(\eta)$  to  $f(\eta), g(\eta), \theta(\eta)$  and  $\phi(\eta)$ . Using Taylor's expansion we write

$$f(\eta, p) = f_0(\eta) + \sum_{m=1}^{\infty} f_m(\eta) p^m, \tag{42}$$

$$g(\eta, p) = g_0(\eta) + \sum_{m=1}^{\infty} g_m(\eta) p^m, \tag{43}$$

$$\theta(\eta, p) = \theta_0(\eta) + \sum_{m=1}^{\infty} \theta_m(\eta) p^m, \tag{44}$$

$$\phi(\eta, p) = \phi_0(\eta) + \sum_{m=1}^{\infty} \phi_m(\eta) p^m, \tag{45}$$

$$\begin{aligned} f_m(\eta) &= \frac{1}{m!} \left. \frac{\partial^m f(\eta; p)}{\partial p^m} \right|_{p=0}, g_m(\eta) = \frac{1}{m!} \left. \frac{\partial^m g(\eta; p)}{\partial p^m} \right|_{p=0}, \\ \theta_m(\eta) &= \frac{1}{m!} \left. \frac{\partial^m \theta(\eta; p)}{\partial p^m} \right|_{p=0}, \phi_m(\eta) = \frac{1}{m!} \left. \frac{\partial^m \phi(\eta; p)}{\partial p^m} \right|_{p=0}, \end{aligned} \tag{46}$$

where the parameters  $\hat{h}_f, \hat{h}_g, \hat{h}_\theta$  and  $\hat{h}_\phi$  have a key role in the convergence of series solutions. The values of parameters are chosen in such a manner that Eqs. (42)–(45) converge at  $p=1$ . Hence Eqs. (42)–(45) give

$$f(\eta) = f_0(\eta) + \sum_{m=1}^{\infty} f_m(\eta), \tag{47}$$

$$g(\eta) = g_0(\eta) + \sum_{m=1}^{\infty} g_m(\eta), \tag{48}$$

$$\theta(\eta) = \theta_0(\eta) + \sum_{m=1}^{\infty} \theta_m(\eta), \tag{49}$$

$$\phi(\eta) = \phi_0(\eta) + \sum_{m=1}^{\infty} \phi_m(\eta). \tag{50}$$

The general solutions are arranged as follows

$$f_m(\eta) = f_m^*(\eta) + C_1 + C_2 e^\eta + C_3 e^{-\eta} \tag{51}$$

$$g_m(\eta) = g_m^*(\eta) + C_4 + C_5 e^\eta + C_6 e^{-\eta} \tag{52}$$

$$\theta_m(\eta) = \theta_m^*(\eta) + C_7 e^\eta + C_8 e^{-\eta} \tag{53}$$

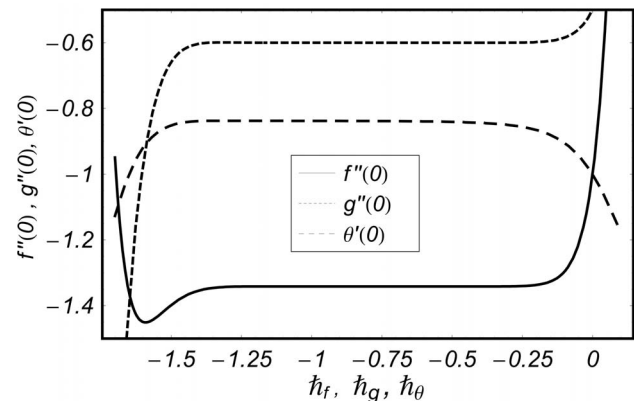
$$\phi_m(\eta) = \phi_m^*(\eta) + C_9 e^\eta + C_{10} e^{-\eta} \tag{54}$$

in which the special solutions are denoted by  $f_m^*, g_m^*, \theta_m^*$  and  $\phi_m^*$ .

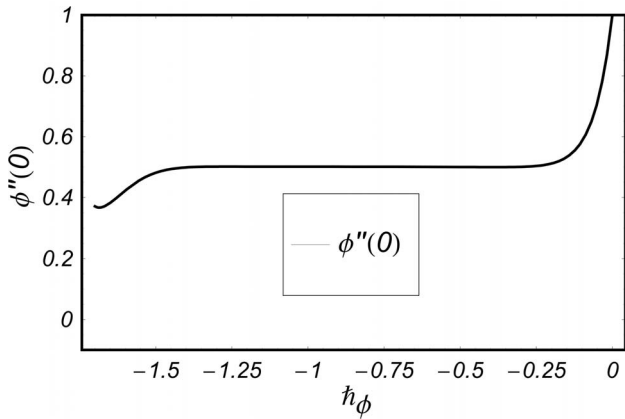
### Convergence of Series Solutions and Discussion

It is well known fact that the homotopy analysis method has a great freedom to choose the auxiliary parameters  $\hat{h}_f, \hat{h}_g, \hat{h}_\theta$  and  $\hat{h}_\phi$  for adjusting and controlling the convergence of series solutions. To determine the appropriate convergence interval of the constructed series solutions, the  $\hat{h}$ -curves at 17<sup>th</sup>-order of approximations are sketched. Figs. 2 and 3 clearly show that the range of admissible values of  $\hat{h}_f, \hat{h}_g, \hat{h}_\theta$  and  $\hat{h}_\phi$  are  $-1.30 \leq \hat{h}_f \leq -0.2, -1.40 \leq \hat{h}_g \leq -0.15, -1.40 \leq \hat{h}_\theta \leq -0.4$  and  $-1.35 \leq \hat{h}_\phi \leq -0.25$ .

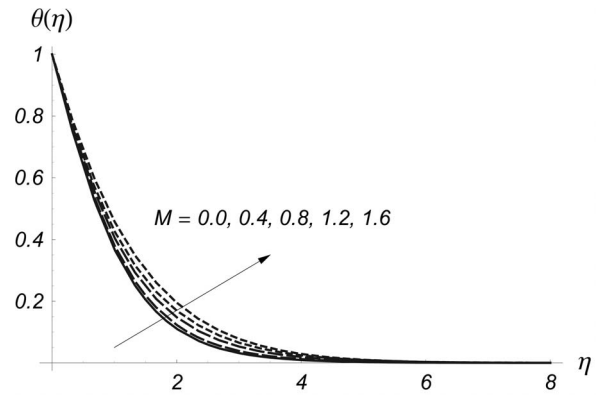
The results are displayed graphically to see the effects of  $\beta, M, \alpha, s, r, B$  and  $Pr$  on the prescribed surface temperature and prescribed surface heat flux. We denote temperature variation for PST case by  $\theta(\eta)$  and for PHF situation by  $\phi(\eta)$  in the Figs. 4–17. Figs. 4 and 5 illustrate the variations of Deborah number on  $\theta(\eta)$  and  $\phi(\eta)$ . From these Figs., we have seen that both  $\theta(\eta)$  and  $\phi(\eta)$  are increased with an increase in  $\beta$ . Deborah number is based on the relaxation time. When Deborah number increases, the relaxation time increases. This increase in relaxation time causes an increase in  $\theta(\eta)$  and  $\phi(\eta)$ . Comparison of Figs. 4 and 5 shows that  $\beta$  has similar effects on  $\theta(\eta)$  and  $\phi(\eta)$ . Figs. 6 and 7 are plotted to see the effects of magnetic parameter  $M$  on  $\theta(\eta)$  and  $\phi(\eta)$ . Clearly the thermal boundary layer thicknesses are increased for larger values of magnetic parameter. In fact the magnetic parameter involves the Lorentz force. Larger values of magnetic parameter correspond to the stronger Lorentz force. This stronger Lorentz force give rise to the thermal boundary layer thicknesses.



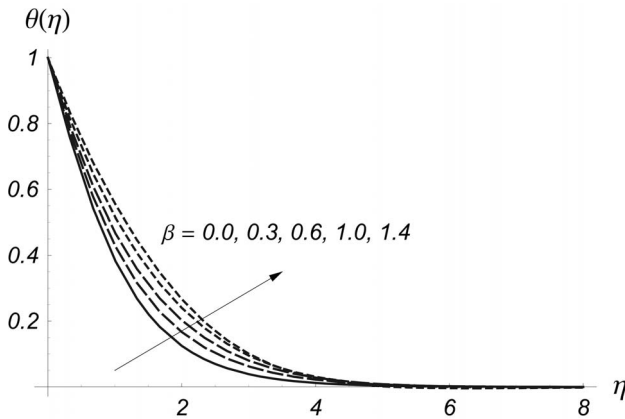
**Figure 2.**  $\hat{h}$ -curves for the functions  $f(\eta), g(\eta)$  and  $\theta(\eta)$  when  $\beta=0.1, M=0.7, \alpha=0.5, Pr=1.4, r=s=0.4$  and  $B=0.3$ . doi:10.1371/journal.pone.0068139.g002



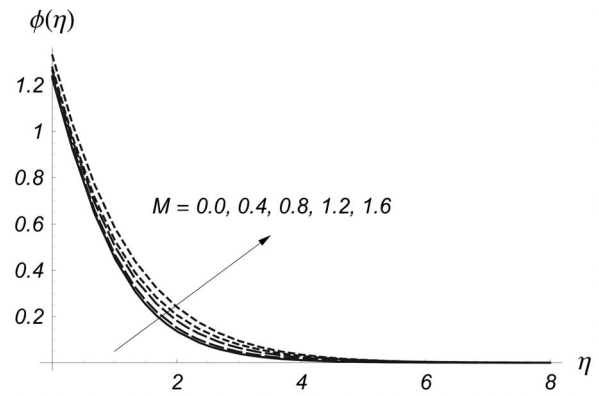
**Figure 3.**  $h$ - curve for the function  $\phi(\eta)$  when  $\beta=0.1$ ,  $M=0.7$ ,  $\alpha=0.5$ ,  $Pr=1.4$ ,  $r=s=0.4$  and  $B=0.3$ .  
doi:10.1371/journal.pone.0068139.g003



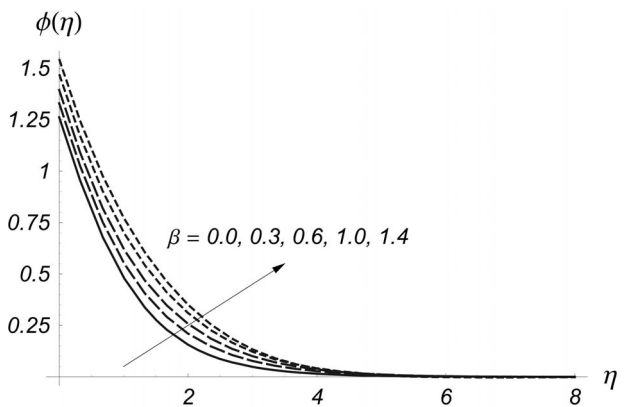
**Figure 6.** Influence of  $M$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $\alpha=0.5$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g006



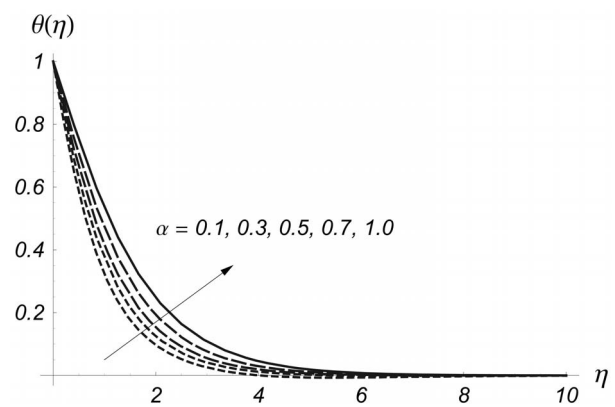
**Figure 4.** Influence of  $\beta$  on  $\theta(\eta)$  when  $M=0.7$ ,  $\alpha=0.5$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g004



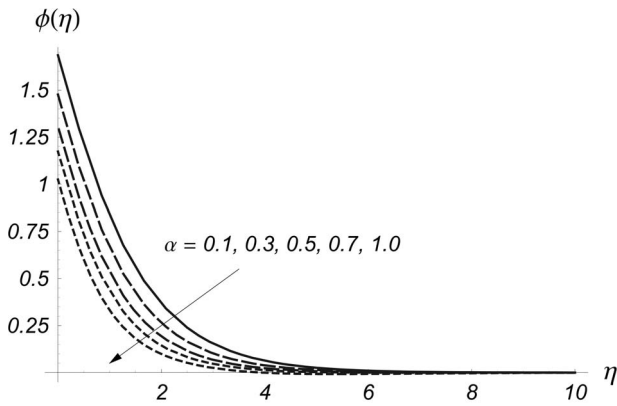
**Figure 7.** Influence of  $M$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $\alpha=0.5$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g007



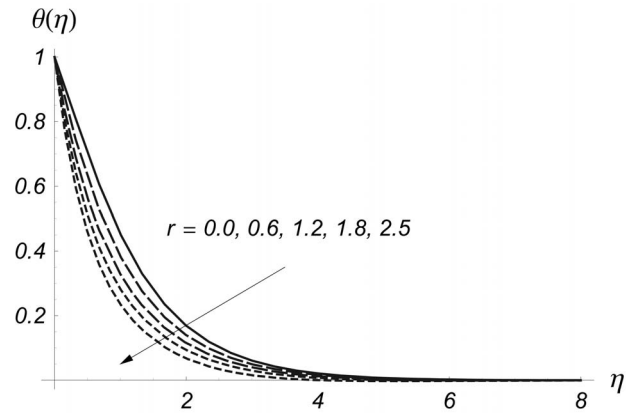
**Figure 5.** Influence of  $\beta$  on  $\phi(\eta)$  when  $M=0.7$ ,  $\alpha=0.5$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g005



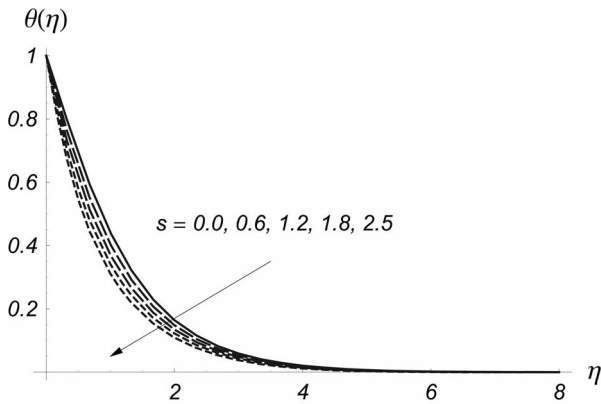
**Figure 8.** Influence of  $\alpha$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g008



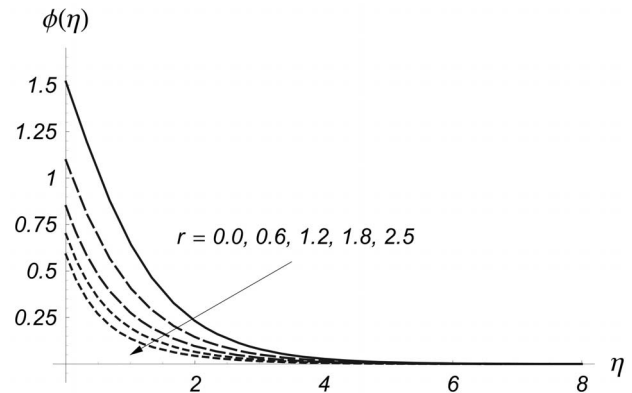
**Figure 9.** Influence of  $\alpha$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $s=0.4$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g009



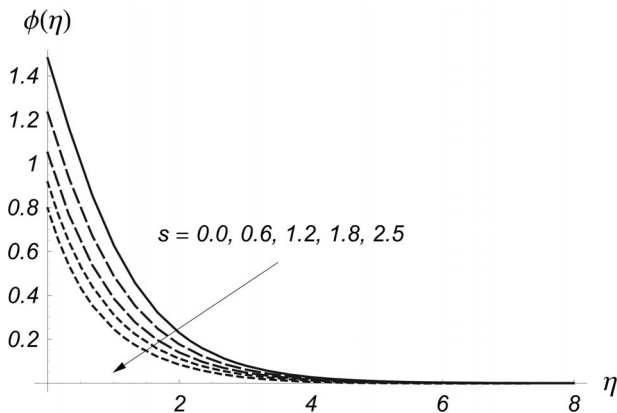
**Figure 12.** Influence of  $r$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $s=0.4$ ,  $\alpha=0.5$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g012



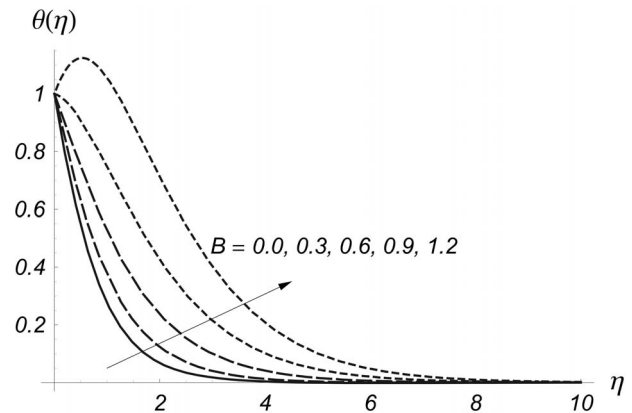
**Figure 10.** Influence of  $s$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $\alpha=0.5$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g010



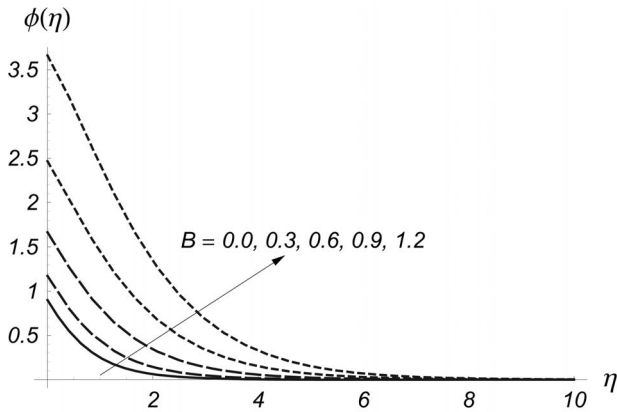
**Figure 13.** Influence of  $r$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $s=0.4$ ,  $\alpha=0.5$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g013



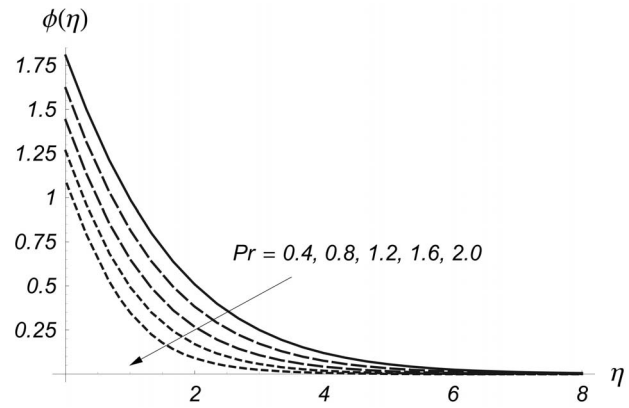
**Figure 11.** Influence of  $s$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $r=0.3$ ,  $\alpha=0.5$  and  $B=0.4$ .  
doi:10.1371/journal.pone.0068139.g011



**Figure 14.** Influence of  $B$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $s=0.4$ ,  $\alpha=0.5$  and  $r=0.3$ .  
doi:10.1371/journal.pone.0068139.g014



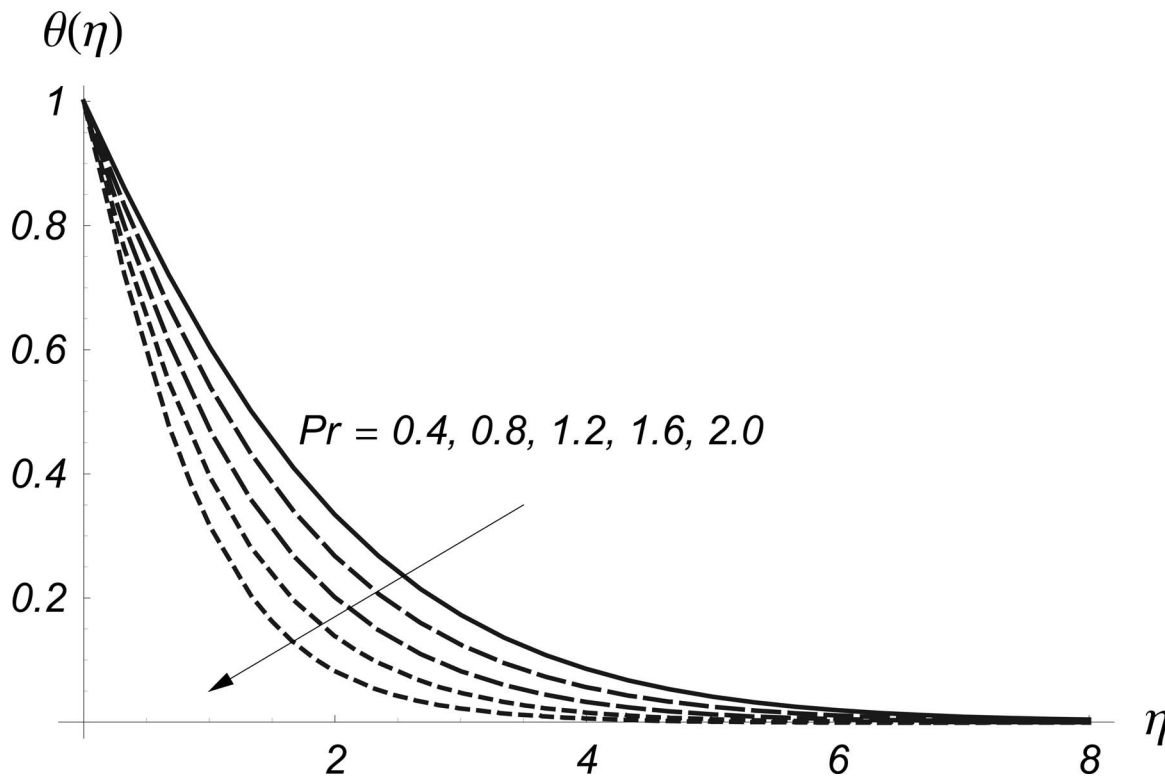
**Figure 15. Influence of  $B$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $Pr=1.5$ ,  $s=0.4$ ,  $\alpha=0.5$  and  $r=0.3$ .**  
doi:10.1371/journal.pone.0068139.g015



**Figure 17. Influence of  $Pr$  on  $\phi(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $B=0.4$ ,  $r=0.3$ ,  $\alpha=0.5$  and  $s=0.4$ .**  
doi:10.1371/journal.pone.0068139.g017

Figs. 8 and 9 illustrate the variations of  $\alpha$  on  $\theta(\eta)$  and  $\phi(\eta)$ . From these Figs. it is noticed that both  $\theta(\eta)$  and  $\phi(\eta)$  are reduced when we increased the values of  $\alpha$ . Also the thermal boundary layer becomes thinner for higher values of  $\alpha$ . This reduction in thermal boundary layer for larger values of  $\alpha$  is due to the entertainment of cooler to ambient fluid. The power indices  $r$  and  $s$  control the non-uniformity of the surface temperature in the prescribed surface temperature situation. Figs. 10 and 11 depict that  $\theta(\eta)$  and  $\phi(\eta)$  are decreasing functions of  $s$ . Also we noted that  $\phi(\eta)$  reduces rapidly as comparison to  $\theta(\eta)$ . Effect of  $r$  on  $\theta(\eta)$  and  $\phi(\eta)$  are seen in the Figs. 12 and 13. The values of  $\theta(\eta)$  and  $\phi(\eta)$  are reduced when values of  $r$  are increased. It is concluded that the non-

uniformity of the sheet temperature has prominent effect on the temperature fields for the reduction in temperature and thinner thermal boundary layer. Comparison of Figs. 12 and 13 illustrates that the variations in  $\phi(\eta)$  are more pronounced when compared to the variations in  $\theta(\eta)$ . Also we examined that  $\phi(\eta)$  at the wall reduced rapidly when the values of  $r$  are larger. Figs. 14 and 15 depict the variations of heat generation/absorption parameter  $B$  on  $\theta(\eta)$  and  $\phi(\eta)$ . Both  $\theta(\eta)$  and  $\phi(\eta)$  are increased by increasing values of heat generation/absorption parameter. Physically an increase in heat generation/absorption parameter produced more heat due to which the temperature of fluid increases. This increase in temperature gives rise to  $\theta(\eta)$  and  $\phi(\eta)$ . The effects of Prandtl number on  $\theta(\eta)$  and  $\phi(\eta)$  are analyzed in the Figs. 16 and 17.



**Figure 16. Influence of  $Pr$  on  $\theta(\eta)$  when  $\beta=0.2$ ,  $M=0.7$ ,  $B=0.4$ ,  $r=0.3$ ,  $\alpha=0.5$  and  $s=0.4$ .**  
doi:10.1371/journal.pone.0068139.g016



**Table 1.** Convergence analysis of series solutions by numerical data for different order of deformations when  $\beta=0.1, M=0.7, \alpha=0.5, Pr=1.4, r=s=0.4, B=0.3$  and  $\hat{h}_f = \hat{h}_g = \hat{h}_0 = \hat{h}_\phi = -0.9$ .

Order of deformations	$f''(0)$	$g''(0)$	$\theta'(0)$	$\phi'(0)$
1	-1.345900	-0.592325	-0.92800	0.55000
10	-1.341759	-0.600119	-0.84012	0.50038
16	-1.341761	-0.600122	-0.83823	0.50111
25	-1.341761	-0.600122	-0.83775	0.50128
30	-1.341761	-0.600122	-0.83775	0.50128
35	-1.341761	-0.600122	-0.83775	0.50128
40	-1.341761	-0.600122	-0.83775	0.50128

doi:10.1371/journal.pone.0068139.t001

**Table 2.** Temperature gradient at surface  $\theta'(0)$  for different values of  $\alpha, r$  and  $s$  with  $\beta_1 = \beta_2 = \beta = 0.0$  and  $Pr = 1.0$ .

		$r=s=0$	$r=-2, s=0$	$r=2, s=0$	$r=0, s=-2$	$r=0, s=2$
[23]	$\alpha=0.25$	-0.665933	0.554512	-1.364890	-0.413111	-0.883125
[24]		-0.665927	0.554573	-1.364890	-0.413101	-0.883123
Present		-0.66593	0.55457	-1.36489	-0.41310	-0.88312
[23]	$\alpha=0.50$	-0.735334	0.308578	-1.395356	-0.263381	-1.106491
[24]		-0.735333	0.308590	-1.395357	-0.263376	-1.106500
Present		-0.73533	0.30858	-1.39536	-0.26338	-1.10649
[23]	$\alpha=0.75$	-0.796472	0.135471	-1.425038	-0.126679	-1.292003
[24]		-0.796470	0.135470	-1.425037	-0.126679	-1.292010
Present		-0.79472	0.13547	-1.42504	-0.12667	-1.29200

doi:10.1371/journal.pone.0068139.t002

These Figs. clearly show that  $\theta(\eta), \phi(\eta)$  and their related thermal boundary layer thicknesses are reduced for the larger values of Prandtl number Pr. Obviously the Prandtl number depends upon the thermal diffusivity. Larger values of Prandtl number give

smaller thermal diffusivity and consequently the values of  $\theta(\eta)$  and  $\phi(\eta)$  decrease.

Table 1 has been prepared to analyze the convergent values of the velocities,  $\theta(\eta)$  and  $\phi(\eta)$ . We have seen that our solutions for velocities converge from 16th order of approximations whereas one needs 25th order of deformations for  $\theta(\eta)$  and  $\phi(\eta)$ . Hence we need less deformations for the velocities in comparison to temperatures for a convergent solution. Table 2 provides the values of temperature gradient  $\theta'(0)$  for different values of  $\alpha, r$  and  $s$  when  $\beta = M = 0$  and  $Pr = 1.0$ . One can see that our solutions has an excellent agreement with the previous results in a limiting case [20,21]. Further, it is observed that the temperature gradient at surface  $\theta'(0)$  becomes positive and reduces for  $r = -2.0$  and  $s = 0$  and negative for  $r = 0$  and  $s = -2.0$ . Table 3 presents the numerical values of  $\theta'(0)$  and  $\phi(0)$  for different values of Pr and B when  $\beta = M = 0, r = s = 1.0$  and  $\alpha = 0.25$ . From this Table we noted that our series solutions have very good agreement with the previous results available in the literature.

### Concluding Remarks

In this study, the three-dimensional MHD flow of Maxwell fluid generated by bidirectional stretching surface is investigated for two cases of prescribed surface temperature (PST) and prescribed surface heat flux (PHF). The effects of applied magnetic field  $B_0$  are also taken into account. Interesting observations of this study can be mentioned below:

- Effects of Deborah number  $\beta_1$  on  $\theta(\eta)$  and  $\phi(\eta)$  are similar in a qualitative manner.
- Both  $\theta(\eta)$  and  $\phi(\eta)$  are increasing functions of magnetic parameter  $M$ .
- Increase in ratio parameter  $\alpha$  reduces the temperatures and their boundary layer thicknesses.
- Temperature for  $\phi(\eta)$  case decreases rapidly in comparison to  $\theta(\eta)$  case when larger values of  $r$  and  $s$  are employed.
- An increase in heat generation/absorption parameter enhances the temperatures  $\theta(\eta)$  and  $\phi(\eta)$ .
- Our series solutions have an excellent agreement with the previous results in limiting cases.

**Table 3.** Temperature gradient at surface  $\theta'(0)$  and  $\phi(0)$  for different values of Pr and B when  $M = \beta = 0, r = s = 1.0$  and  $\alpha = 0.5$ .

		$-\theta'(0)$ for PST			$\phi(0)$ for PHF		
		$B = -0.2$	$B = 0.0$	$B = 0.2$	$B = -0.2$	$B = 0.0$	$B = 0.2$
[23]	Pr = 1.0	1.348064	1.255781	1.148932	0.741805	0.796317	0.870355
[24]		1.348064	1.255780	1.148934	0.741808	0.796318	0.870372
Present		1.34806	1.25578	1.14893	0.74180	0.79632	0.87037
[23]	Pr = 5.0	3.330392	3.170979	3.002380	0.300265	0.315360	0.333069
[24]		3.330394	3.170981	3.002384	0.300265	0.315363	0.333071
Present		3.33039	3.17098	3.00238	0.30028	0.31537	0.33308
[23]	Pr = 10.0	4.812149	4.597141	4.371512	0.207807	0.217527	0.228754
[24]		4.812151	4.597143	4.371516	0.207809	0.217529	0.228756
Present		4.81215	4.59714	4.37152	0.20781	0.21753	0.22876

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## Author Contributions

Conceived and designed the experiments: SAS AA TH. Performed the experiments: SAS AA TH. Analyzed the data: SAS AA TH. Contributed

reagents/materials/analysis tools: SAS AA TH. Wrote the paper: SAS AA TH.

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