Regulation of Harvester Ant Foraging as a Closed-Loop Excitable System

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S1 Text. Effect of volatility on the frequency of oscillations in the FN.

Here we use results from [1] Chapter III, Theorem 3 to obtain an asymptotic expansion for the period of the limit cycle $T_{LC}$ as $\epsilon_2$ goes to zero. We show that the period of the FN limit cycle is inversely proportional to $c$ by computing the leading term in the expansion.

The limit cycle of the FN is comprised of four components: two fast components that stretch along the $v$ direction between the crest and valley of the cubic nullcline, and two slow components that stretch along the sides of the cubic nullcline. Because it takes much longer to traverse the slow components of the limit cycle than the fast components of the cycle, the period can be approximated by the time it takes trajectories to traverse the two slow components. These slow components run from $v = -2$ to $v = -1$ and from $v = 2$ to $v = 1$, respectively, and are proportional to the length of the sides of the cubic nullcline, which we show are proportional to $c$.

**Theorem 1.** The limit cycle of the FN system

$$\epsilon_1 \epsilon_2 \frac{dv}{dt} = v - v^3/3 - cu - 0.35 + s$$
$$\epsilon_1 \frac{du}{dt} = v - cu$$

has the asymptotic representation:

$$T_{LC} = T_0 + C_1 \epsilon_2^{2/3} + C_2 \epsilon_2 \ln \frac{1}{\epsilon_2} + O(\epsilon_2),$$

as $\epsilon_2 \to 0$, where $C_1$ and $C_2$ are constants and where

$$T_0 = \frac{3\epsilon_1}{c} \left\{ \int_{-2}^{-1} \frac{(v^2 - 1)}{(3z - v^3)} dv + \int_{2}^{1} \frac{(v^2 - 1)}{(3z - v^3)} dv \right\}.$$

**Proof.** By Chapter III, Theorem 3 of [1], the limit cycle of the FN model has the asymptotic representation

$$T_{LC} = T_0 + C_1 \epsilon_2^{2/3} + C_2 \epsilon_2 \ln \frac{1}{\epsilon_2} + C_3 \epsilon_2 + O(\epsilon_2^{4/3}).$$

Or, equivalently,

$$T_{LC} = T_0 + C_1 \epsilon_2^{2/3} + C_2 \epsilon_2 \ln \frac{1}{\epsilon_2} + O(\epsilon_2).$$

Let time be scaled by $1/\epsilon_1$ and let $z = s - 0.35$, leading to the new system

$$\epsilon_2 \frac{dv}{dt} = v - v^3/3 - cu + z$$
$$\frac{du}{dt} = v - cu$$

The critical manifold of this fast-slow system is $M_0 := \{(v, u) \in \mathbb{R}^2 | u = (v - v^3/3 + z)/c\}$. In the limit $\epsilon_2 \to 0$, the slow manifold is equal to the critical manifold. Let $\Psi_0$ denote the limit cycle in this limit.

Using the description of $M_0$ as a graph $u = h(v)$, the dynamics of the system on the slow flow can be written as

$$\frac{du}{dt} = v^3/3 - z.$$
We get a second expression for \( \frac{du}{dt} \) by differentiating \( M_0 \) with respect to \( t \)
\[
\frac{du}{dt} = \frac{1 - v^2}{c} \frac{dv}{dt}.
\]
Equating the two expressions we obtain
\[
\frac{dv}{dt} = \frac{c(v^3 - 3z)}{3(1 - v^2)}.
\]
Multiplying both sides by \( dt \) and integrating over \( \Psi_0 \),
\[
T_0 = \frac{3}{c} \int_{\Psi_0} \frac{(1 - v^2)}{(v^3 - 3z)} dv.
\]
In \( \Psi_0 \), the fast components of the orbit take place instantaneously and the time taken to complete the orbit is equal to the time taken to traverse the slow components. The slow components of the trajectory take place on the slow manifold between \( v \in [-2, -1] \) and \( v \in [1, 2] \), yielding the expression
\[
T_0 = \frac{3\epsilon_1}{c} \left\{ \int_{-2}^{-1} \frac{(1 - v^2)}{(v^3 - 3z)} dv + \int_{1}^{2} \frac{(1 - v^2)}{(v^3 - 3z)} dv \right\}
\]
where time has been scaled back to its original form. This expression is inversely proportional to \( c \). Furthermore, this integral has a short closed form solution when the slow components are symmetric (i.e. \( z = 0 \), or \( s = 0 \)),
\[
T_0 = 2 \frac{3\epsilon_1}{c} \int_{-2}^{-1} \frac{(1 - v^2)}{v^4} dv = \frac{\epsilon_1}{4c} (-9 + 8 \log 8).
\]
We compute the constants \( C_1 \) and \( C_2 \) by applying formulas 7.9 and 7.10 of [1] Chapter III, Theorem 3. When \( s = 0.35 \), the flow along the system is symmetric and the constants \( C_1 \) and \( C_2 \) are given by
\[
C_1 = \frac{3.79366\epsilon_1}{e^{1/3}}
\]
and
\[
C_2 = -\frac{\epsilon_1}{2}.
\]
When \( s \neq 0.35 \), \( z \neq 0 \) and the flow along the system is not symmetric. In this case the constants \( C_1 \) and \( C_2 \) can each be represented as the sum of two constants, and the asymptotic representation for \( T_0 \) becomes
\[
T_{LC} = T_0 + (C_{11} + C_{12})\epsilon_2^{2/3} + (C_{21} + C_{22})\epsilon_2 \ln \frac{1}{\epsilon_2} + O(\epsilon_2)
\]
where
\[
C_{11} = \frac{3.37214|1 - 3z| \text{ Sgn}(1/3 - z)}{(-8/9 + z(-7/3 + z))(c/\epsilon_2^2)^{1/3}},
\]
\[
C_{12} = \frac{\epsilon_1(-2 + 6z + |1 - 3z|)}{2(1 - 3z)^2},
\]
\[
C_{21} = \frac{3.37214|1 - 3z| \text{ Sgn}(1/3 + z)}{(-8/9 + z(-7/3 + z))(c/\epsilon_2^2)^{1/3}},
\]
\[
C_{22} = \frac{\epsilon_1(-2 - 6z + |1 + 3z|)}{2(1 + 3z)^2}
\]
and Sgn represents the sign function.

References